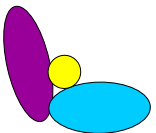
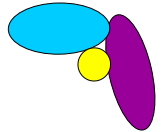


BALL-TYPE MODELS

- Overview
- PFC: fundamentals and applications
- OVAL, EDEM, YADE
- other applications



OVERVIEW OF DEM SOFTWARES



Quasi-static methods

← *an equilibrium state is searched for*

From an initial approximation of the equilibrium state searched for, the displacements \mathbf{u} are to be determined taking the system to the equilibrium (assumption: time-independent behaviour, zero accelerations!!!)

$$" \mathbf{K} \cdot \Delta \mathbf{u} + \mathbf{f} = \mathbf{0} "$$

- Kishino, 1988
 - Bagi-Bojtár, 1991
- } *circular, perfectly rigid elements, deformable contacts*

Time-stepping methods

" $\mathbf{M} \cdot \mathbf{a}(t) = \mathbf{f}(t, \mathbf{u}(t), \mathbf{v}(t))$ " ← *a process in time is searched for*

simulate the motion of the system along small, but finite Δt timesteps

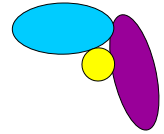
Explicit timestepping methods:

- UDEC *deformable polyhedral elements, deformable contacts*
- BALL-type models, e.g. PFC *rigid elements, deformable contacts*

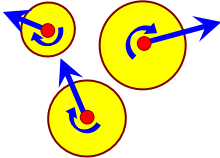
Implicit timestepping methods:

- DDA („Discontinuous Deformation Analysis”) *deformable polyhedral elements*
- contact dynamics models *rigid elements, non-deformable contacts*

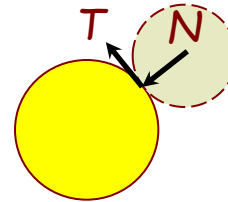
BALL-TYPE MODELS



BALL: P.A. Cundall, 1979

elements:  2D, perfectly rigid;

contacts: point-like;
Coulomb friction



$$\mathbf{u}^p(t) = \begin{bmatrix} u_x^p(t) \\ u_y^p(t) \\ \varphi_z^p(t) \end{bmatrix}$$

eqs of motion:

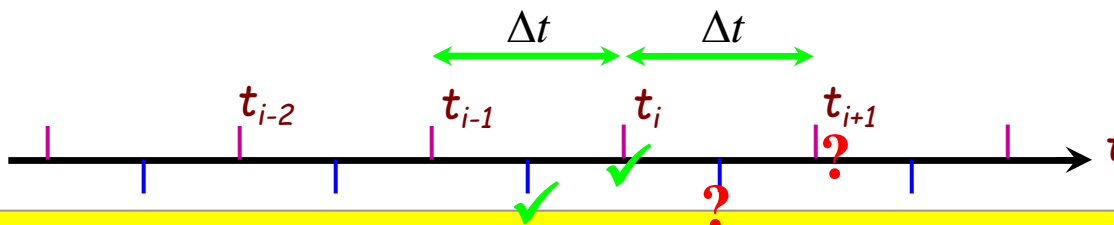
$$\mathbf{M}^p(t) \mathbf{a}^p(t) = \mathbf{f}^p(t, \mathbf{u}(t), \mathbf{v}(t))$$

$$\mathbf{M}^p = \begin{bmatrix} m^p & & \\ & m^p & \\ & & I^p \end{bmatrix}$$

$$\begin{cases} m^p a_x^p = f_x^p \\ m^p a_y^p = f_y^p \\ I^p \beta_z^p = m_z^p \end{cases}$$

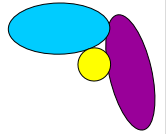
numerical solution:
method of central differences

$$\mathbf{v}^p(t_i + \Delta t/2) = \mathbf{v}^p(t_i - \Delta t/2) + (\mathbf{M}^p)^{-1} \mathbf{f}^p(t_i) \Delta t$$

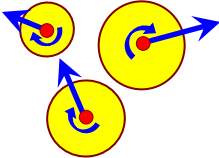


positions
forces, stresses
accelerations
velocities

BALL-TYPE MODELS

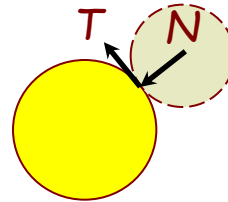


BALL: P.A. Cundall, 1979

elements:  2D, perfectly rigid;

$$\mathbf{u}^p(t) = \begin{bmatrix} u_x^p(t) \\ u_y^p(t) \\ \varphi_z^p(t) \end{bmatrix}$$

contacts: point-like;
Coulomb friction



eqs of motion:

$$\mathbf{M}^p(t)\mathbf{a}^p(t) = \mathbf{f}^p(t, \mathbf{u}(t), \dot{\mathbf{u}}(t))$$

numerical solution:
method of central differences

$$v_x^p(t_i + \Delta t/2) = v_x^p(t_i - \Delta t/2) + \frac{f_x^p(t_i)}{m^p} \Delta t$$

$$u_x^p(t_i + \Delta t) = u_x^p(t_i) + v_x^p(t_i + \Delta t/2) \cdot \Delta t$$

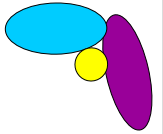
$$v_y^p(t_i + \Delta t/2) = v_y^p(t_i - \Delta t/2) + \frac{f_y^p(t_i)}{m^p} \Delta t$$

$$u_y^p(t_i + \Delta t) = u_y^p(t_i) + v_y^p(t_i + \Delta t/2) \cdot \Delta t$$

$$\omega_z^p(t_i + \Delta t/2) = \omega_z^p(t_i - \Delta t/2) + \frac{m_z^p(t_i)}{I^p} \Delta t$$

$$\varphi_z^p(t_i + \Delta t) = \varphi_z^p(t_i) + \omega_z^p(t_i + \Delta t/2) \cdot \Delta t$$

BALL-TYPE MODELS



BALL: P.A. Cundall, 1979

3D version: 1983, TRUBAL

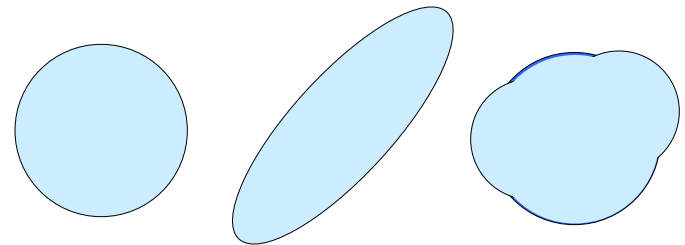
NSF grant, free for anyone who asks for

⇒ huge effect on granular mechanics researches !!!

„BALL-type” models:

→ perfectly rigid elements

→ shape: to have point-like contacts



→ eqs of motion: $\mathbf{M}^p(t)\mathbf{a}^p(t) = \mathbf{f}^p(t, \mathbf{u}(t), \dot{\mathbf{u}}(t))$

→ numerical solution of the eqs of motion: explicit time integration,
(mostly: central difference scheme)

BALL-TYPE MODELS

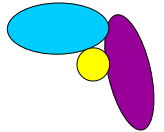
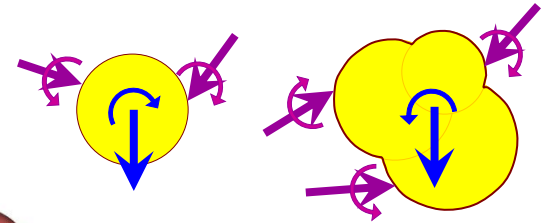
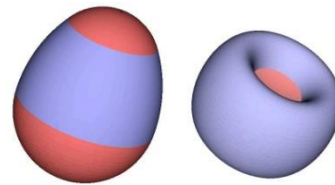
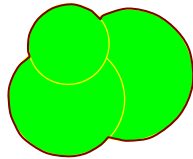
most important codes:

PFC-2D, PFC-3D, P.A. Cundall, Itasca Consulting

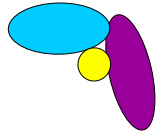
OVAL, M.R. Kuhn, Portland Catholic University

EDEM, J. Favier, Edinburgh

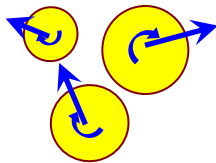
YADE (some versions), French origin, very active international community



PFC BASIC PRINCIPLES

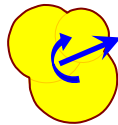


Elements:



perfectly rigid cylinders (2D) or spheres (3D)

m : mass, I : inertia



„clump”: rigid group of elements, fixed together

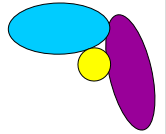
m : sum of masses, I : sum of inertia about
the „centre”

Degrees of freedom:

translation of the „centre” (i.e. reference point);

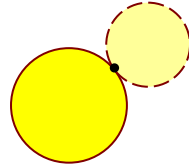
rotation about the „centre”

PFC BASIC PRINCIPLES – THE CONTACTS



Contact types:

frictional



$$\Delta N^c = k_N \Delta u_N^c \quad N^c \leq 0$$

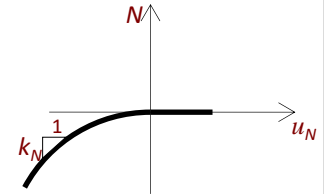
$$\Delta T^c = k_T \Delta u_T^c \quad |T^c| \leq -\mathbf{v} \cdot N^c$$

→ linear: $k_N = \text{konst.}; k_T = \text{konst.}$ ← *default*

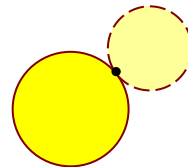
→ Hertz-Mindlin:

$$k_N = \frac{\langle G \rangle \sqrt{2 \langle R \rangle}}{1 - \langle \mu \rangle} \sqrt{u_N^c}$$

$$k_S = \frac{2 \sqrt[3]{3 \langle G \rangle^2 (1 - \langle \mu \rangle) \langle R \rangle}}{2 - \langle \mu \rangle} \sqrt[3]{-N^c}$$



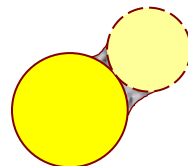
cemented → point-like:



$$N^c \leq N_{\max}$$

$$|T^c| \leq T_{\max}$$

→ extended:



$$\Delta \sigma_N = \tilde{k}_N \Delta u_N \quad (\text{lin.}) \quad \sigma_N \leq \sigma_N^{\max}$$

$$\Delta \sigma_T^c = \tilde{k}_T \Delta u_T^c \quad |\sigma_T| \leq \sigma_T^{\max}$$

Viscoelastic contacts, Softening models, other possibilities, C/C++

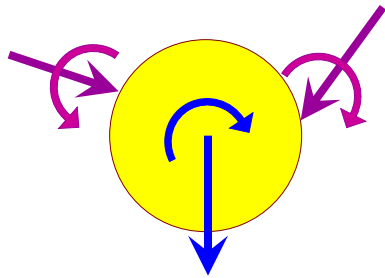
PFC BASIC PRINCIPLES – TIME INTEGRATION



Displacement calculations

Newton II.: „ $ma = f$ ”

– forces acting on the spherical elements:



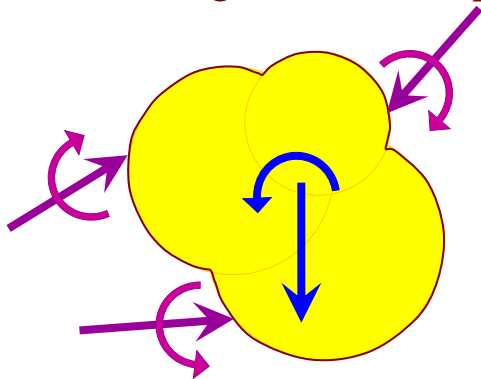
← from the contacts of the element

← from the external loads (weight, drag force)

← from damping

} → f, M

– forces acting on the clumps:



← from the contacts of the element

← from the external loads (weight, drag force)

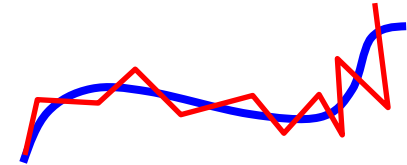
← from damping

} → f, M

PFC BASIC PRINCIPLES – TIME INTEGRATION

Displacement calculations

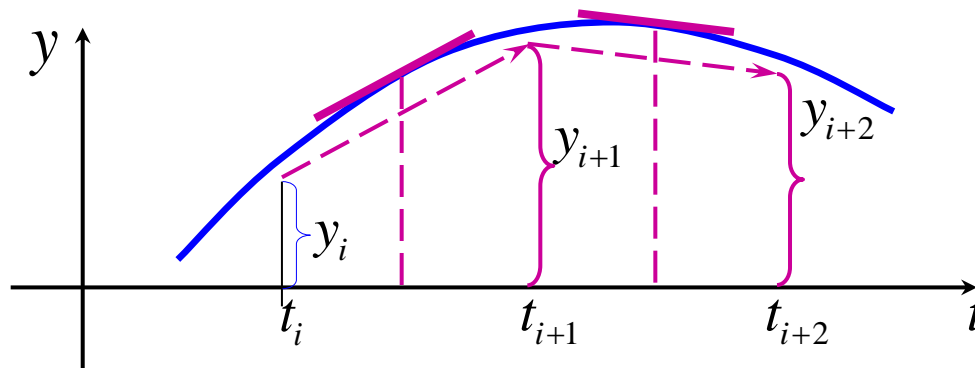
Newton II.: „ $ma = f$ ”



Method of Central Differences

– the eqs of motion, discretized: $\mathbf{v}^p(t_i + \Delta t/2) = \mathbf{v}^p(t_i - \Delta t/2) + (\mathbf{M}^p)^{-1} \mathbf{f}^p(t_i) \Delta t$

– from this: $\mathbf{u}^p(t_i + \Delta t) = \mathbf{u}^p(t_i) + \mathbf{v}^p(t_i + \Delta t/2) \Delta t$



– to ensure numerical stability, and to help fast convergence:

1. estimation for the longest allowed Δt : $\Delta t_{crit} = \min$
2. density scaling: to modify masses/inertia

$$\left\{ \begin{array}{l} \sqrt{m/k^{transl}} \\ \sqrt{I/k^{rotat}} \end{array} \right.$$

for time-dependent problems: never use it!

3. damping

PFC BASIC PRINCIPLES – TIME INTEGRATION



3. Damping:

the eqs. of motion including velocity-proportional damping:

$$\mathbf{v}(t_i + \Delta t/2) = \mathbf{v}(t_i - \Delta t/2) + \mathbf{M}^{-1}(\mathbf{f}(t_i) - c_u \mathbf{v}(t_i - \Delta t/2)) \cdot \Delta t$$

→ 1. Local damping ← *default*

→ 2. Contact viscous damping

PFC BASIC PRINCIPLES – TIME INTEGRATION



3. Damping:

a. *Local damping:* e.g. for a sphere:

$$v_x(t_i + \Delta t/2) = v_x(t_i - \Delta t/2) + \left(f_x(t_i) - \alpha \cdot |f_x(t_i)| \text{sign}(v_x(t_i - \Delta t/2)) \right) \frac{\Delta t}{m}$$

$$\omega_z(t_i + \Delta t/2) = \omega_z(t_i - \Delta t/2) + \left(M_z(t_i) - \alpha \cdot |M_z(t_i)| \text{sign}(\omega_z(t_i - \Delta t/2)) \right) \frac{\Delta t}{I_z}$$

default: $\alpha := 0.70$

- *unequilibrated motions are damped only;*
- *does not depend on the magnitude of the velocities;*
- *very good for systems in which:
parts are already in equilibrium, while parts are still far from the eq.*

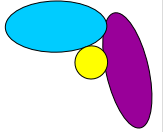
b. *Contact viscous damping:*

viscous force added to the contact force:

its direction: opposite to the relative motion

$$\left\{ \begin{array}{l} |D_N| = c_N \left| \frac{\Delta u_N}{\Delta t} \right| \\ |D_T| = c_T \left| \frac{\Delta u_T}{\Delta t} \right| \end{array} \right.$$

PFC BASIC PRINCIPLES



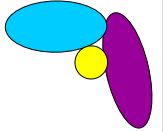
Further details:

e.g. application results, publications, courses, conferences, ...

www.itascacg.com

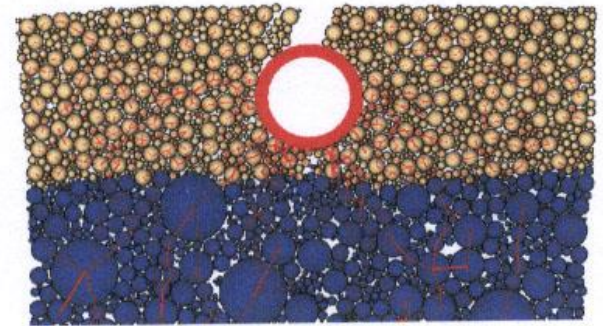
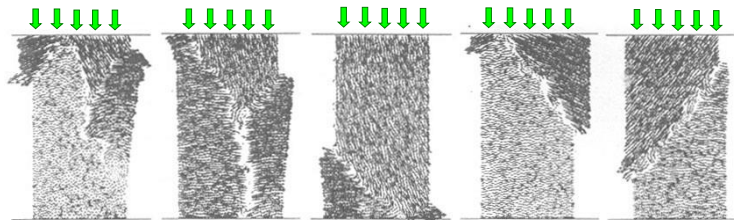
→ Software → Downloads → Demonstration versions

PFC PRACTICAL APPLICATIONS



Usual applications:

loose and cemented granular materials



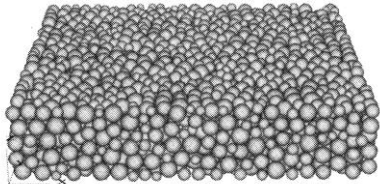
1. Weathering of cemented granular rock under buildings
2. Railway ballast modelling

PFC PRACTICAL APPLICATIONS

Weathering of cemented granular rock

Nova et al, 2004

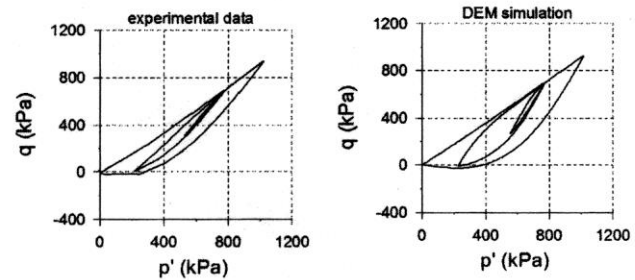
PFC-3D



triaxial loading
3500 elements
size distribution: 1:2

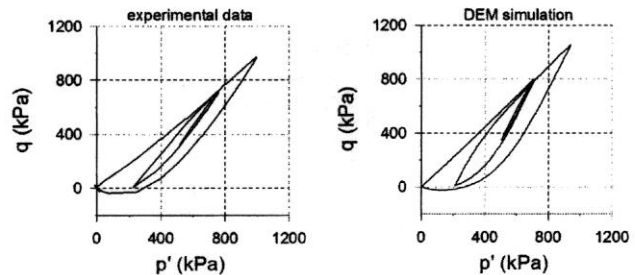
analyzed problem:

weathering of rock under buildings



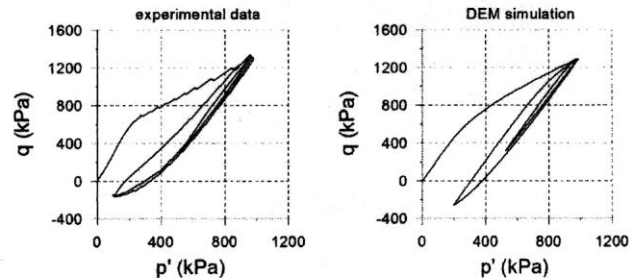
(a) porosity 45% ($D_R = 40\%$)

sand 1.



(b) porosity 39% ($D_R = 90\%$)

sand 2.



(c) porosity 49% (cemented)

cemented

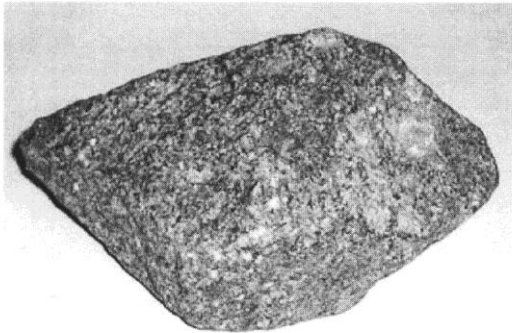
k_H	k_v	μ	c_b	σ'_b	χ	$\frac{\Delta U^p}{U_{lim}^p}$
225 KN/m	135 KN/m	0.2	1500 kPa	250 kPa	0.6	0.2


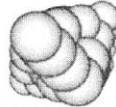
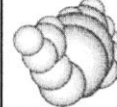
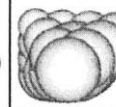

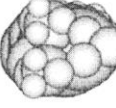

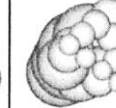
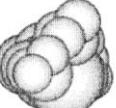
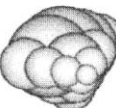

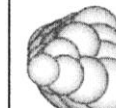
(d) DEM parameters

PFC PRACTICAL APPLICATIONS

Railway ballast modelling

e.g. effect of stone shape: Lu & McDowell, 2007, PFC-3D

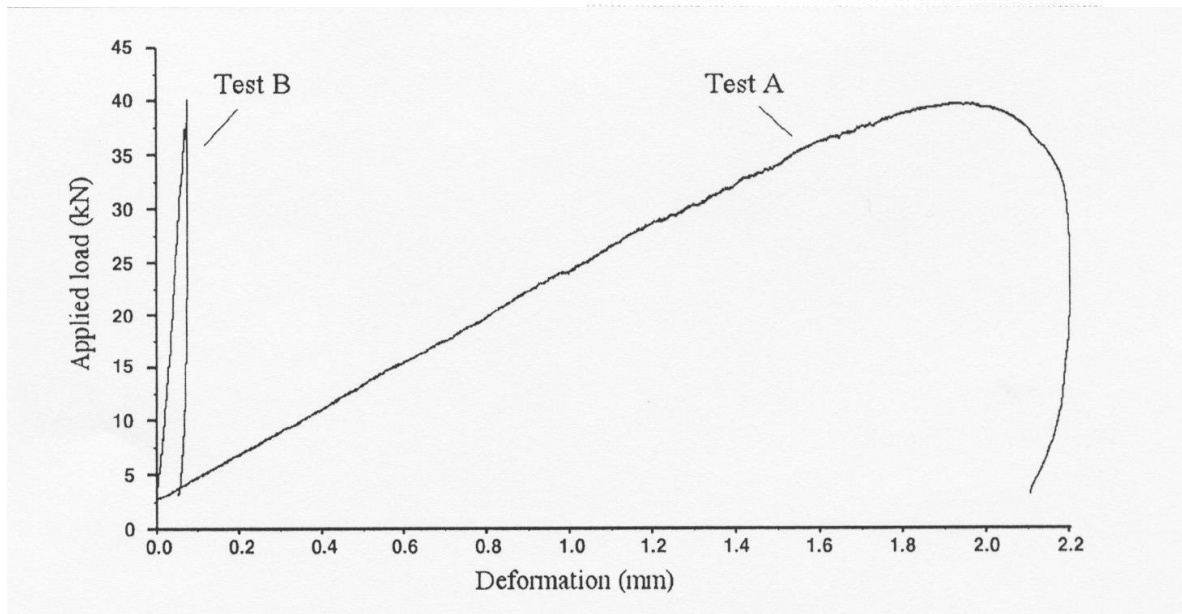
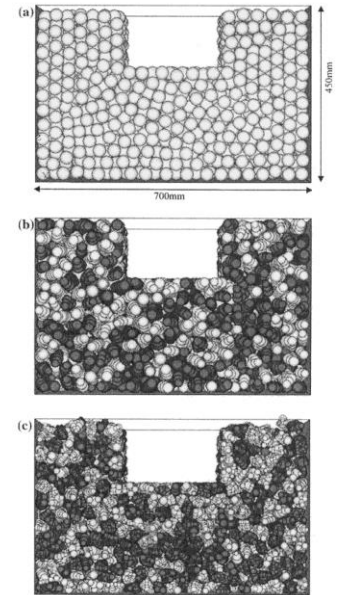
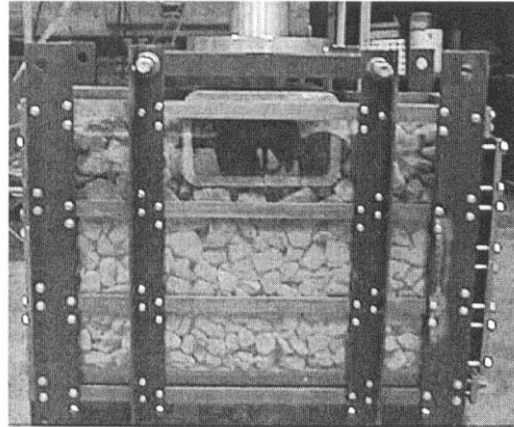


			
19	27	17	19
			
16	27	19	27
			
19	27	19	27

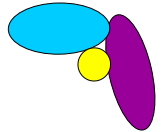
PFC PRACTICAL APPLICATIONS

Railway ballast modelling

e.g. effect of stone shape:
Lu & McDowell, 2007



OVERVIEW OF DEM SOFTWARES



Quasi-static methods

← *an equilibrium state is searched for*

From an initial approximation of the equilibrium state searched for, the displacements \mathbf{u} are to be determined taking the system to the equilibrium (assumption: time-independent behaviour, zero accelerations!!!)

$$" \mathbf{K} \cdot \Delta \mathbf{u} + \mathbf{f} = \mathbf{0} "$$

→ Kishino, 1988

→ Bagi-Bojtár, 1991

} *circular, perfectly rigid elements,
deformable contacts*

Time-stepping methods

" $\mathbf{M} \cdot \mathbf{a}(t) = \mathbf{f}(t, \mathbf{u}(t), \mathbf{v}(t))$ " ← *a process in time is searched for*

simulate the motion of the system along small, but finite Δt timesteps

Explicit timestepping methods:

→ UDEC *deformable polyhedral elements, deformable contacts*

→ BALL-type models, e.g. PFC *rigid elements, deformable contacts*

Implicit timestepping methods:

→ DDA („Discontinuous Deformation Analysis”) *deformable polyhedral elements*

→ contact dynamics models *rigid elements, non-deformable contacts*

BALL-TYPE MODELS

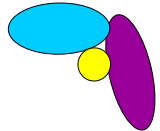
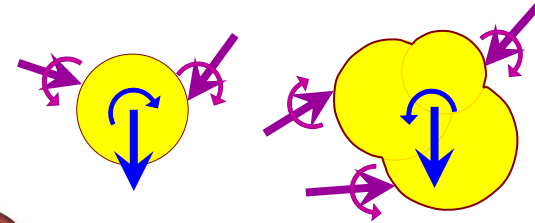
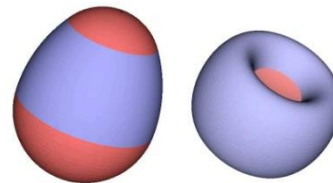
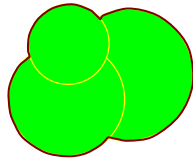
most important codes:

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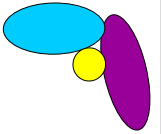
OVAI, M.R. Kuhn, Portland Catholic University

EDEM, J. Favier, Edinburgh

YADE (some versions), French origin, very active international community

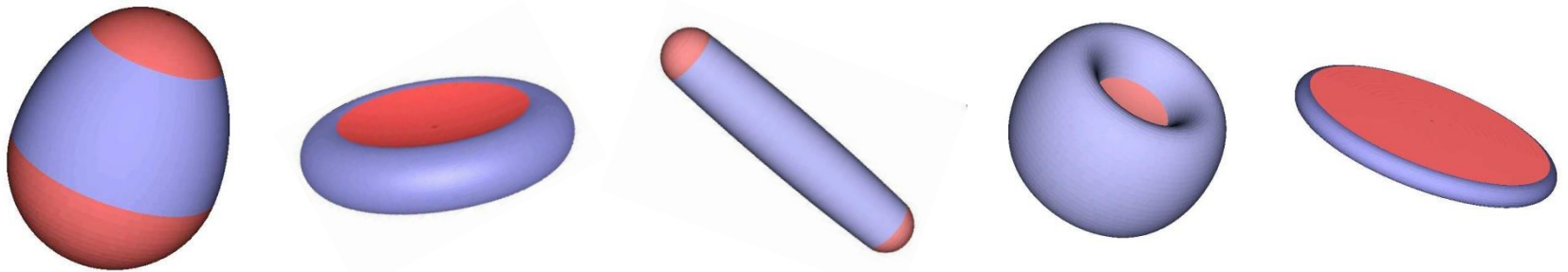


OVAL



Matthew R. Kuhn, USA, Research code!

→ elements: surface composed of cylindrical/spherical/toroidal etc. surfaces



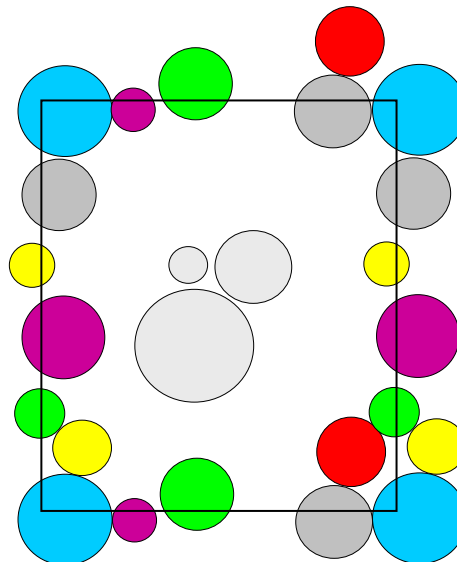
→ contacts:

frictional

→ boundaries: walls; or:

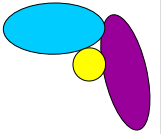
periodic boundaries

→ input: command files,
output: data files, (figures)

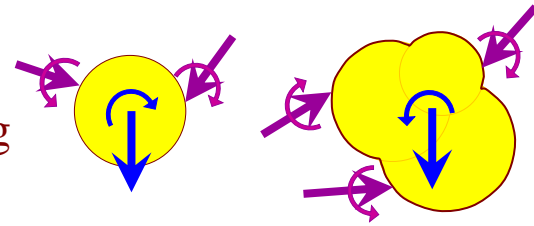


kuhn@up.edu

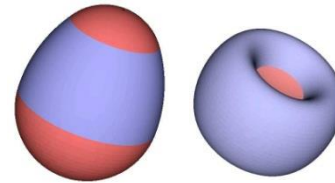
BALL-TYPE MODELS



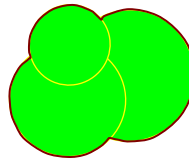
PFC-2D, PFC-3D, P.A. Cundall, Itasca Consulting



OVAL, M.R. Kuhn, Portland Catholic University



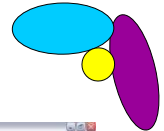
EDEM, J. Favier, Edinburgh



YADE (some versions), French origin, very active international community

EDEM

www.dem-solutions.com

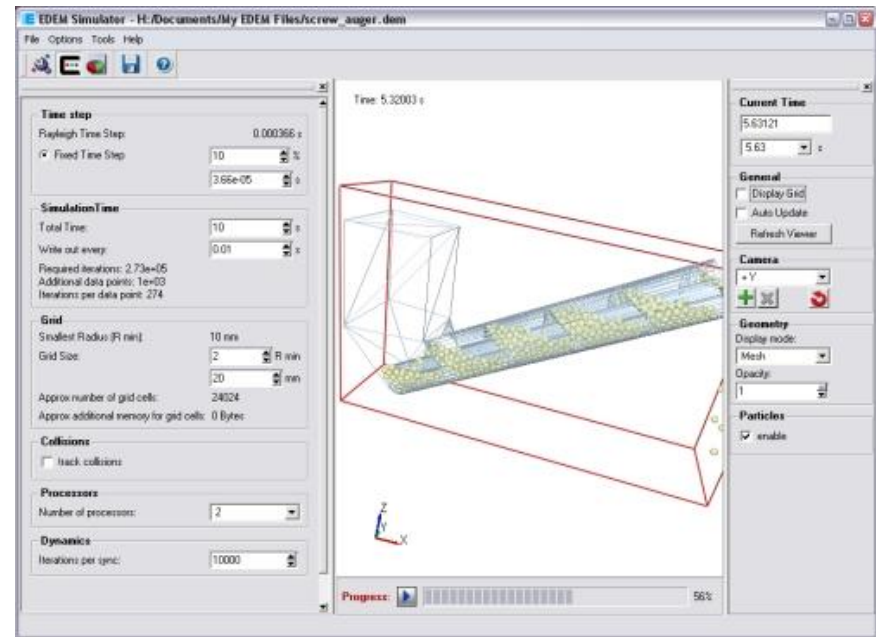
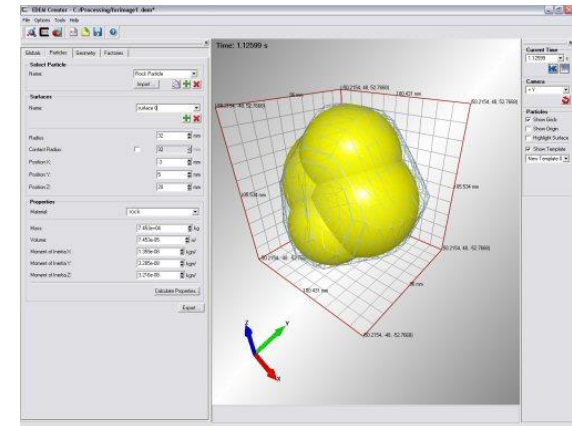


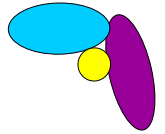
J. Favier, Edinburgh

- elements: spheres / composed of spheres
- contacts: frictional, linearly elastic
Hertz-Mindlin
cohesive
cemented
individually coded

- boundaries: several types!
- special features of the displacement calculations:
 - easy to connect to FEM or CFD (solids, fluids)
 - fast, \\\

→ output: rich (videos, pictures, etc.)

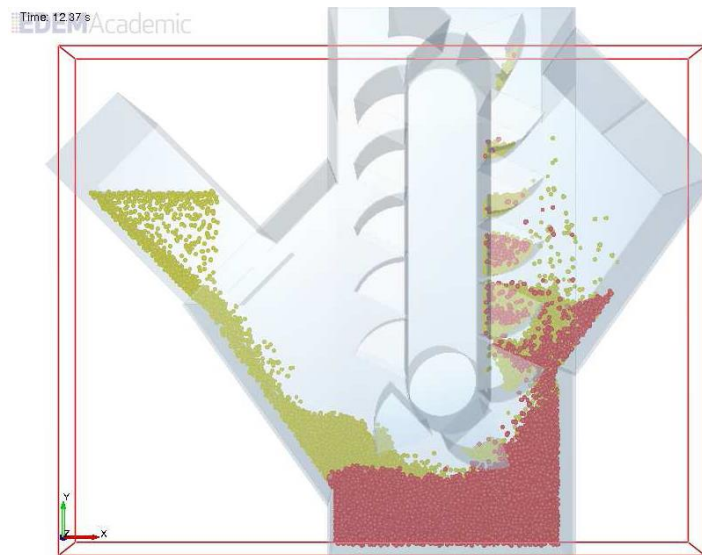
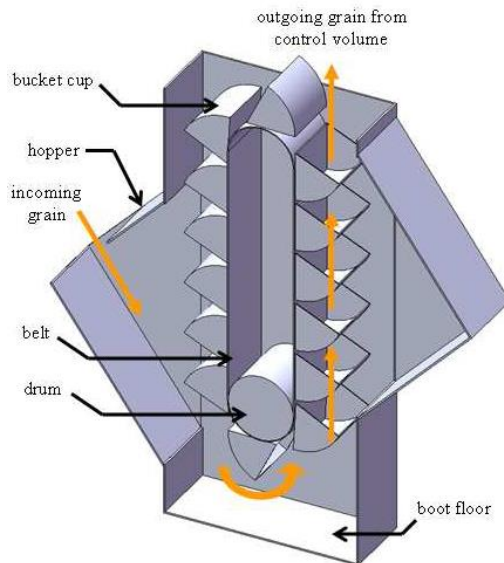
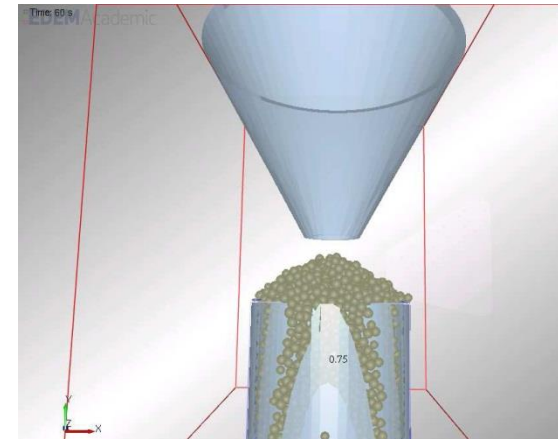
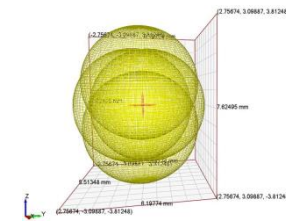
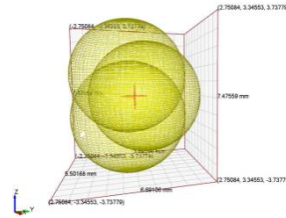




applications:

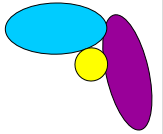
e.g. J. Boac, 2010:
assemblies of soy bean & corn

result:
well-calibrated model
for machine design



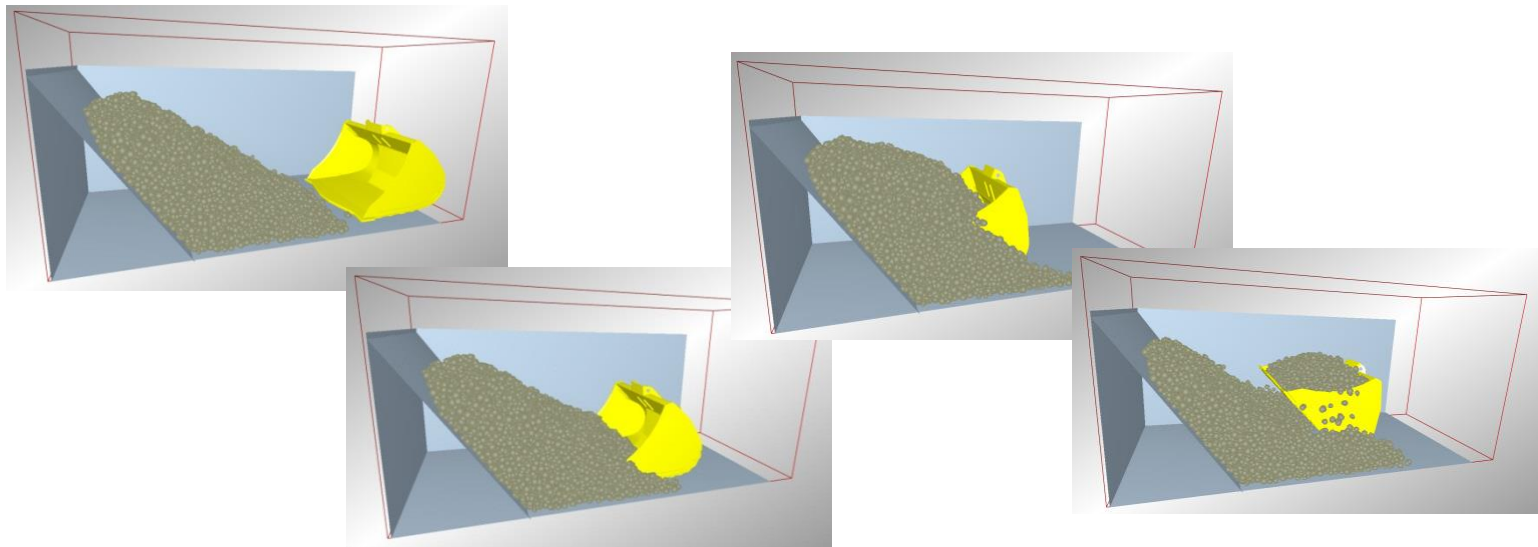
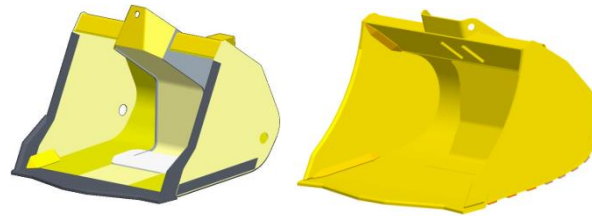
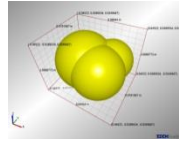
EDEM

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applications:

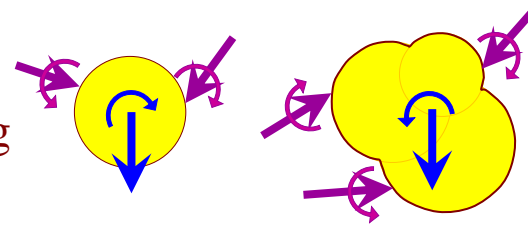
e.g. J. Helgesson, 2010:



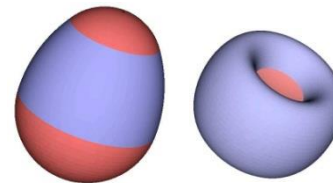
result:
optimize the geometry of the spoon

BALL-TYPE MODELS

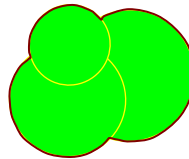
PFC-2D, PFC-3D, P.A. Cundall, Itasca Consulting



OVAL, M.R. Kuhn, Portland Catholic University

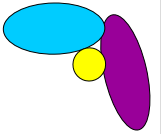


EDEM, J. Favier, Edinburgh



YADE (some versions), French origin, very active international community

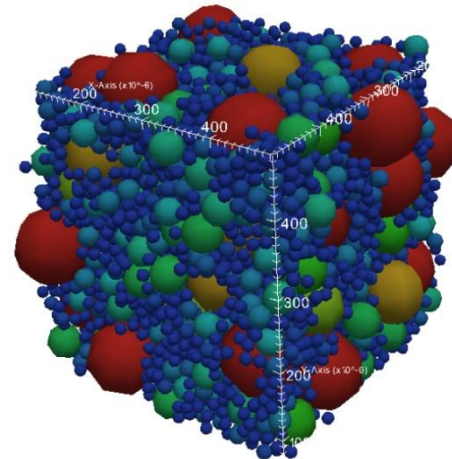
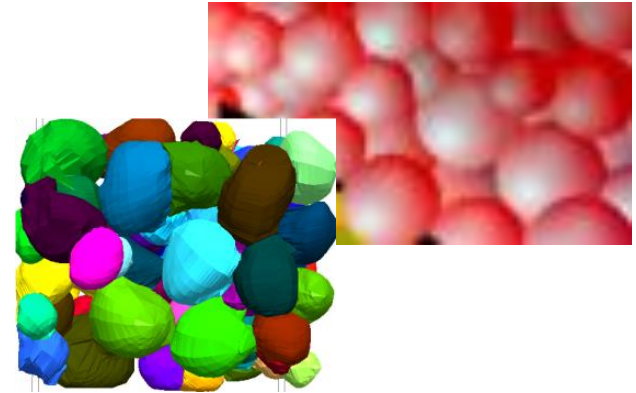
YADE



elements: spheres;
complex shapes consisting of spheres;
polyhedra;
[anything personal can be coded]

contacts:
[several models, individual codes shared]

applications:
researchers!
e.g. simulation of lunar regolith: Modenese (2013)

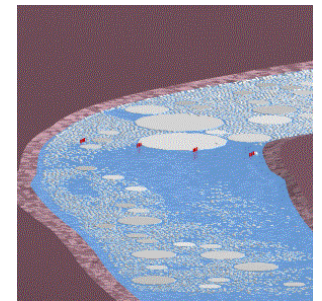
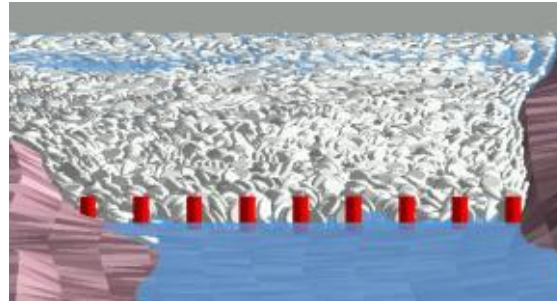
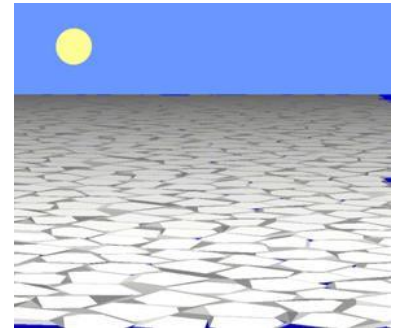


<https://yade-dem.org>

BALL-TYPE MODELS: OTHER APPLICATIONS

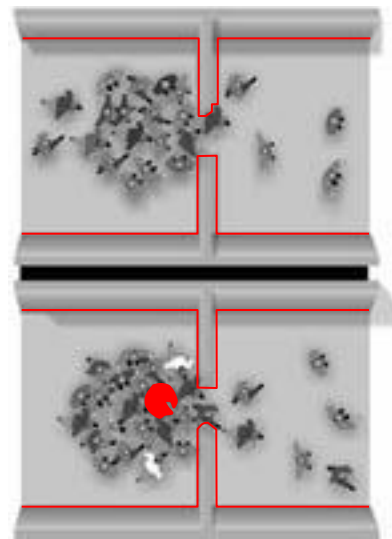
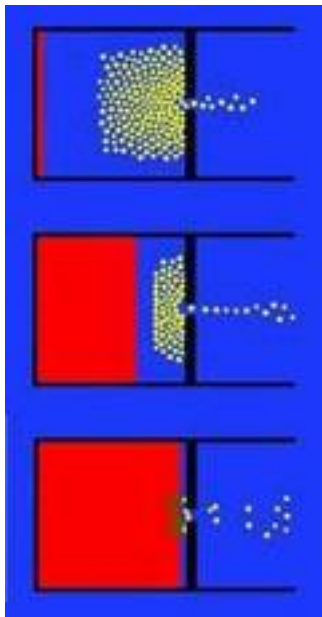
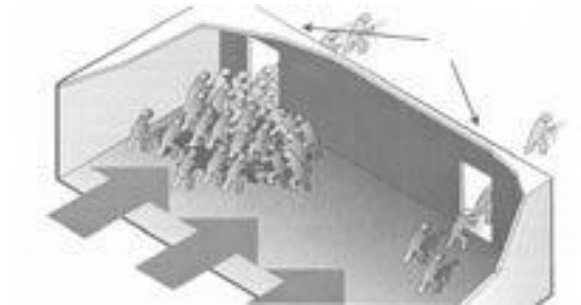
Floating ice blocks: effect on military vessels and structures

US Army Research Institute,
Cold Regions Department:

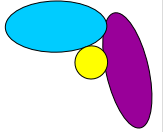


BALL-TYPE MODELS: OTHER APPLICATIONS

Architectural design: Simulation of a crowd in panic



QUESTIONS



1. Under what conditions does a discrete element model belong to the family of BALL-type models?
2. What types of contact models are applied in the BALL-type models? Shortly describe them!
3. Explain the calculation of a single time step in PFC! Why is it important to set a limit to the length of the time step, and how can this limit be estimated?
4. Why should damping be used in BALL-type models? Introduce local damping and contact viscous damping!