



# GRAPHICAL METHODS



## Citation:

K. Bagi (2018): **Mechanics of Masonry Structures**. Course handouts, Department of Structural Mechanics, Budapest University of Technology and Economics

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# THIS LECTURE:

## GRAPHICAL METHODS

Historical times: Practical geometrical rules

e.g. Vitruvius

e.g. Gothic rules

Graphical statics

The basic problem: Stability of an arch

Durand-Claye's stability area method for arches

computerized & extended for domes: Aita et al 2003 ... 2018

Wolfe's method for membrane forces in domes

O'Dwyer's funicular analysis  $\Rightarrow$

Thrust Network Analysis (TNA)

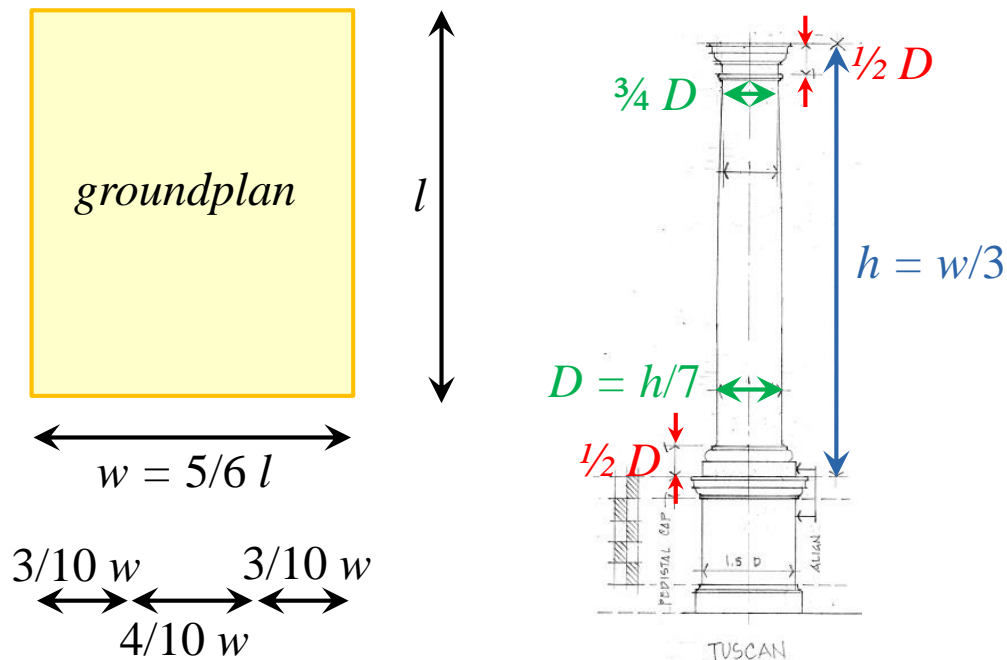
Questions

# Historical times: Practical geometrical rules

Roman era, Vitruvius (Roman Empire, BC 1<sup>st</sup>ct., army engineer & architect):  
„Ten Books on Architecture”

→ inspired many architects, already from VIIIth century;  
particularly important for Renaissance

e.g. in the „Tuscan” order, the design of the *column* of a temple:



St Paul's Church, London, XVIIth century,  
[flickr.com/photos/ddtmmm/1367084017](https://www.flickr.com/photos/ddtmmm/1367084017)

# Historical times: Practical geometrical rules

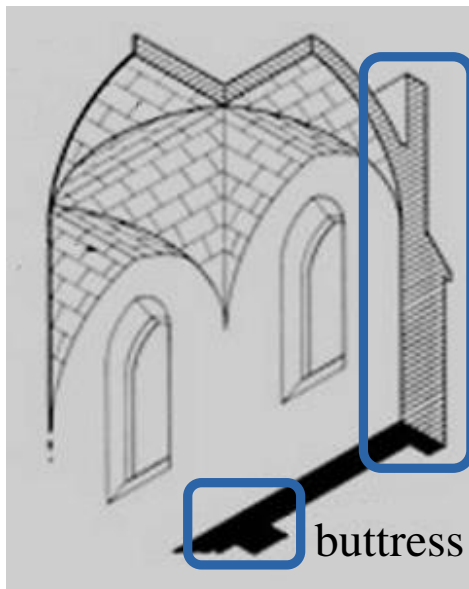
Gothic architecture terminology:

Felicity Lynch: Gothic Art History 1150 - 1500 A.D.

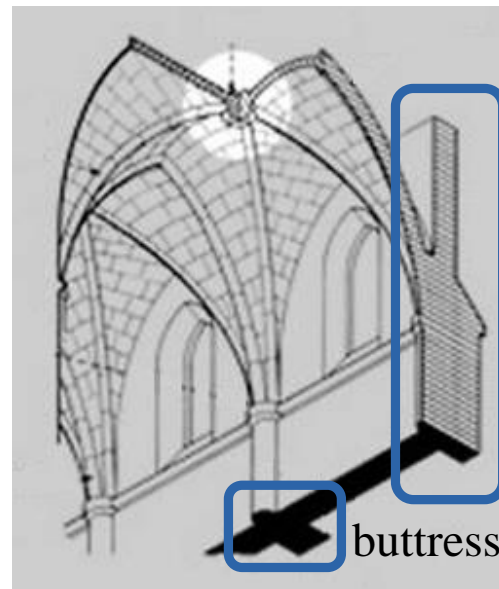
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Cameron Daniels: Architecture of The Middle Ages

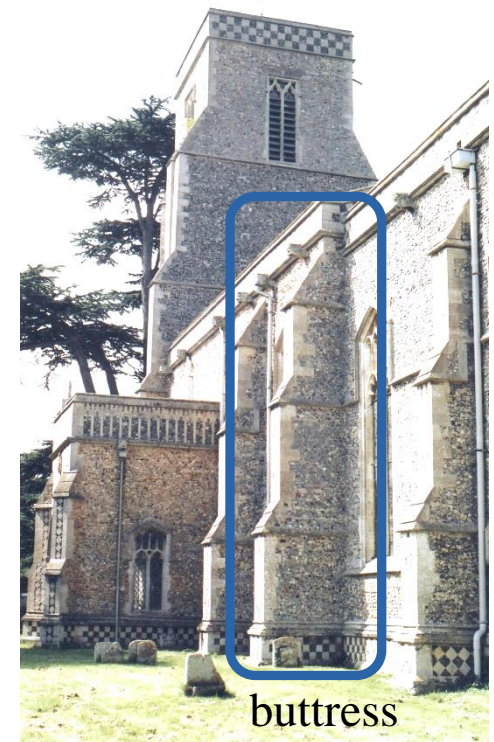
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groin vault



ribbed cross vault

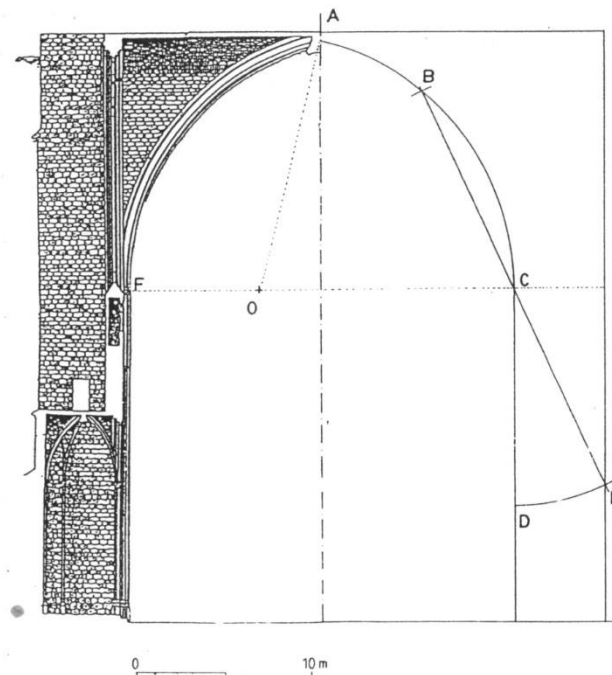
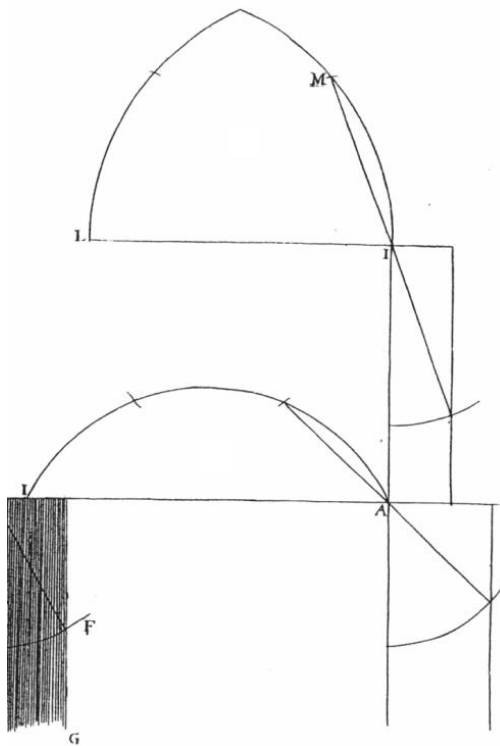


# Historical times: Practical geometrical rules

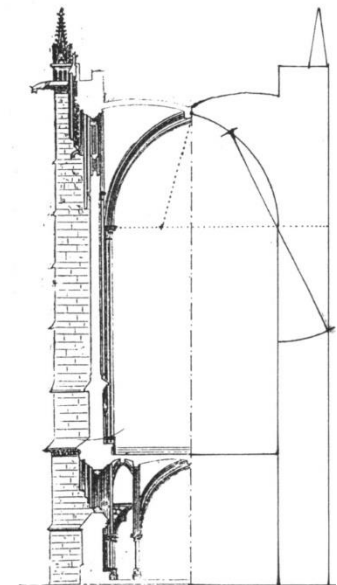
Gothic rules:

e.g. Derand's rule for *buttress thickness*:

(  $\Rightarrow$ . *similarity of Gothic cathedrals of the same geographic area* )



*Gerona cathedral*



*Saint-Chapelle,*

*Paris*

# Historical times: Practical geometrical rules

Gothic rules:

e.g. Rodrigo's interior *pier diameter* design rule:

$$d := \frac{1}{2} \sqrt{h + w + s}$$

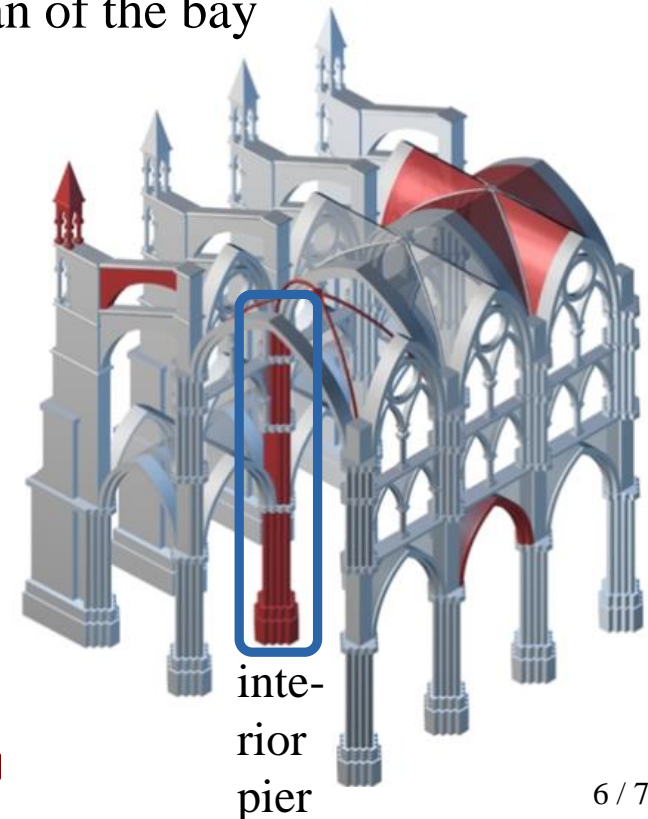
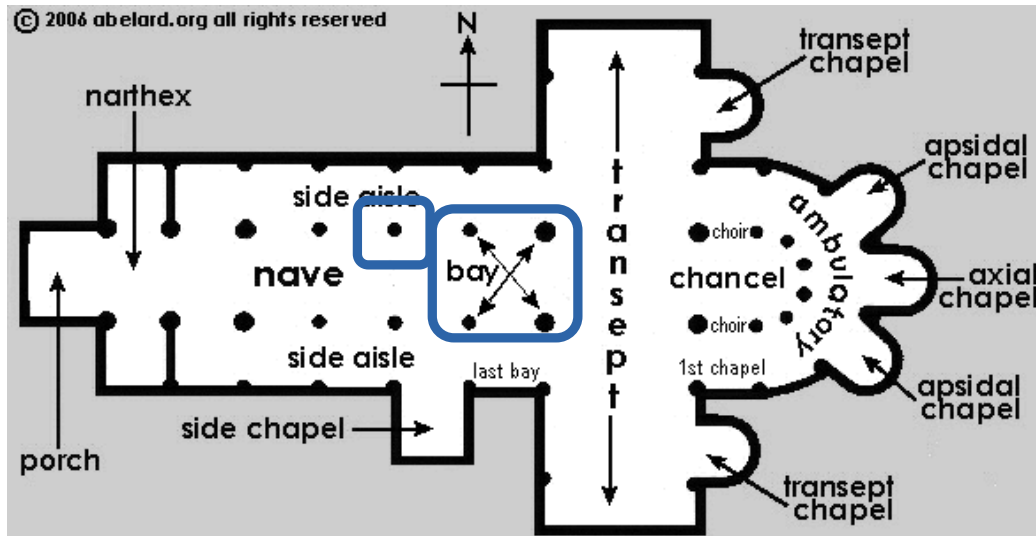
$h$ : pillar height

$w$ : length of the bay

$s$ : span of the bay

dimension !!!!

⇒ works only in Castilian feet (0,28m)



Further reading: Huerta (2006); Aita et al (2018a)

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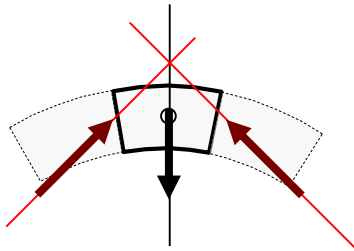
Questions



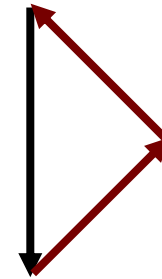
# GRAPHICAL STATICS

Reminder to fundamentals:

Equilibrium of three forces in 2D:



*funicular diagram* („form diagram“):  
the three lines of action intersect



*force diagram*:  
closed vector triangle

Equilibrium of four forces in 3D:

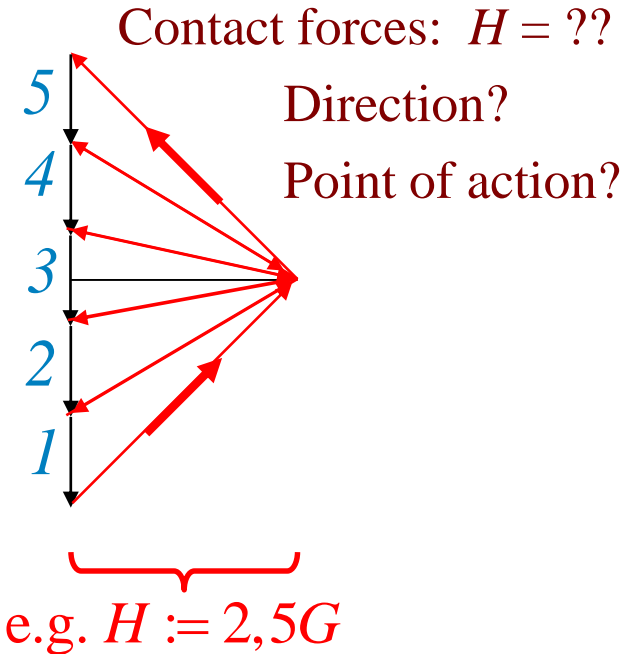
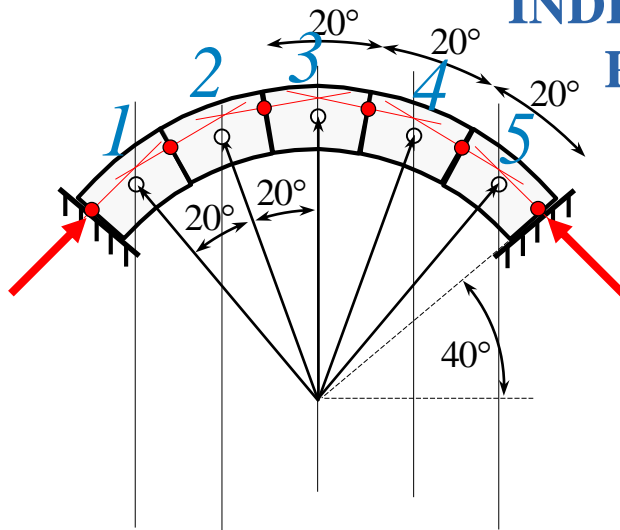
different projections, e.g. hoop view and top view  
all views have to intersect / be closed

More than three (2D) or more than four (3D) forces: closed force diagram,  
but: lines of action not necessarily intersect

# The basic problem: Stability of an arch

Question: arch submitted to its selfweight; ?reactions? ?contact forces?

**3× STATICALLY  
INDETERMINATE  
PROBLEM**



„loads are transmitted to the supports”

Given: geometry:  $R_{inner} = 2,4 \text{ m}$  ;  $R_{middle} = 2,7 \text{ m}$

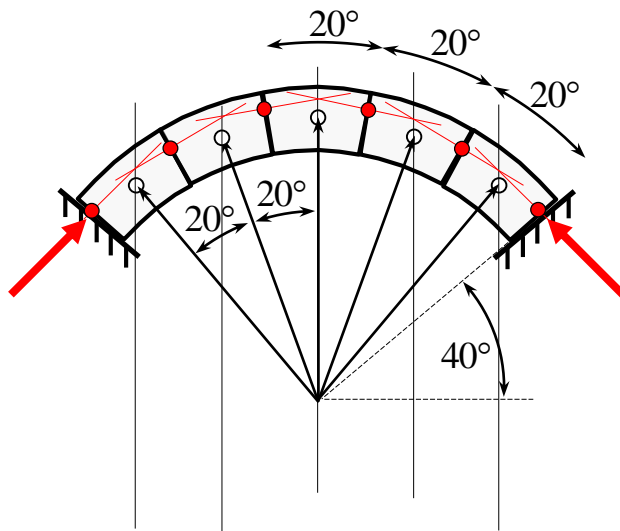
identical selfweight for each block:  $G_1 = G_2 = G_3 = G_4 = G_5$

Try to find an equilibrated force system!

→ contact forces: compression & friction; inside the contact area

# The basic problem: Stability of an arch

Thrust line: [ intuitive concept; theoretical definition: Gáspár et al (2018) ]



≈ „ the line determined by the points of action of the contact forces ”

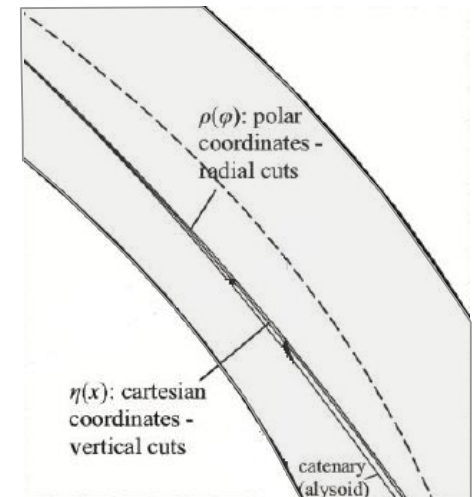
BUT: depends on the orientation of contacts  
(Alexakis & Makris, 2015)

stability criterion: [ later: more details ]

thrust line can be found so that  
it runs everywhere inside the contacts

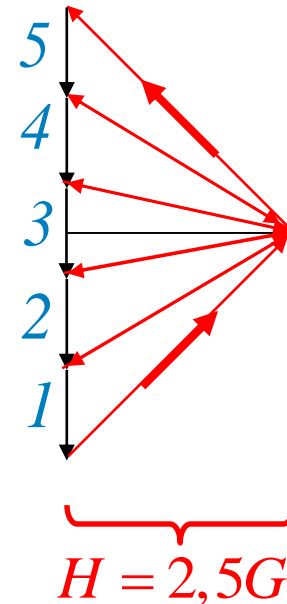
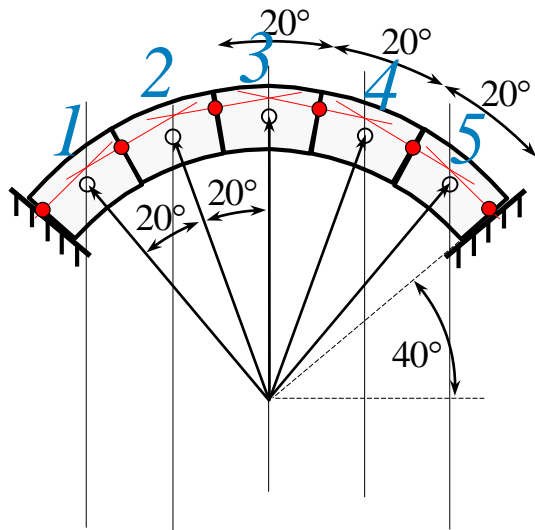
arch shape is „better”, if it can be done with smaller thickness

→ e.g. pointed arch versus circular arch



# The basic problem: Stability of an arch

Question: arch submitted to its selfweight; ?reactions? ?contact forces?



Given: geometry:  $R_{inner} = 2,4 \text{ m}$  ;  $R_{middle} = 2,7 \text{ m}$

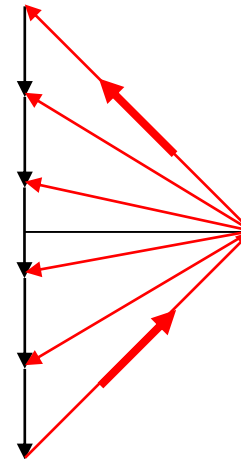
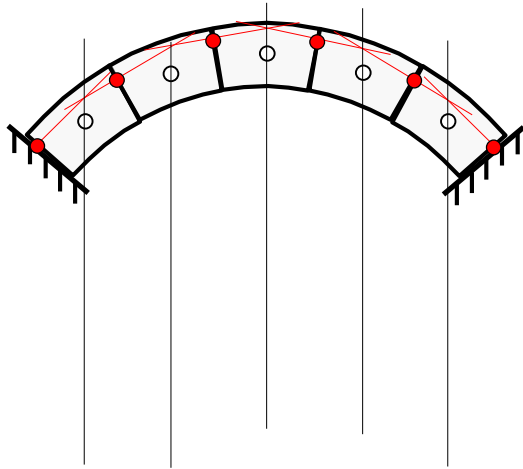
identical selfweight for each block:  $G_1 = G_2 = G_3 = G_4 = G_5$

Try to find an equilibrated force system!

→ contact forces: compression & friction; inside the contact area [kernel?]

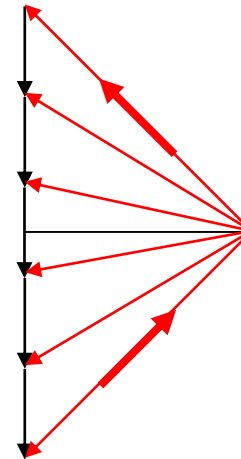
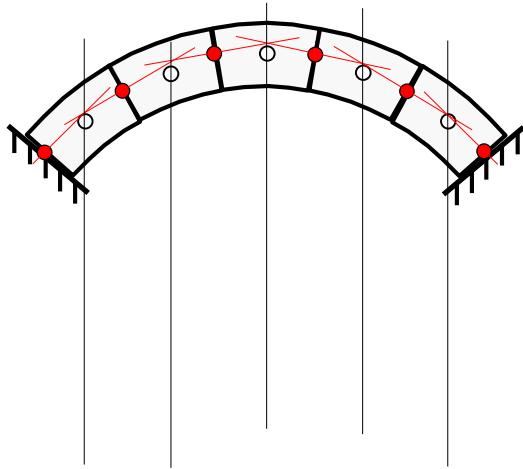
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Question: arch submitted to its selfweight; ?reactions? ?contact forces?



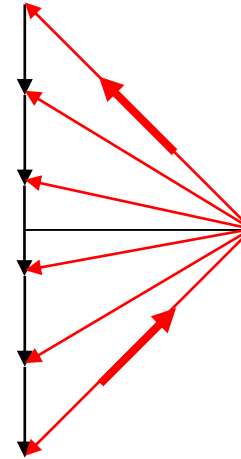
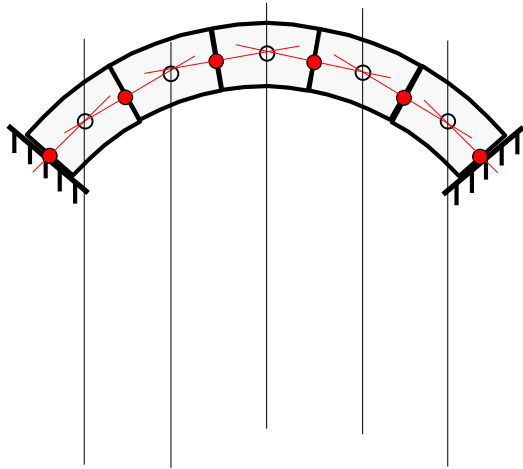
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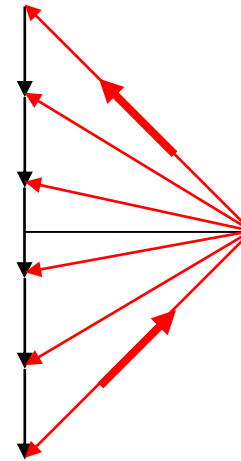
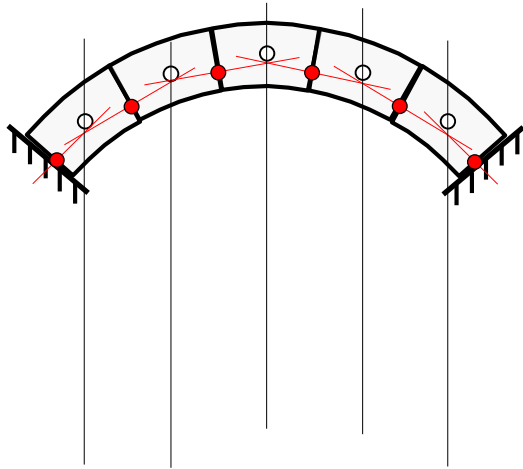
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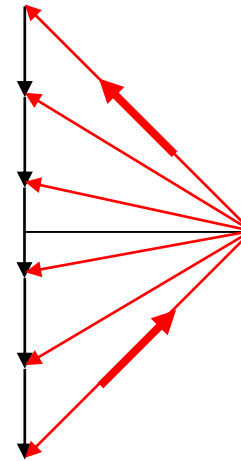
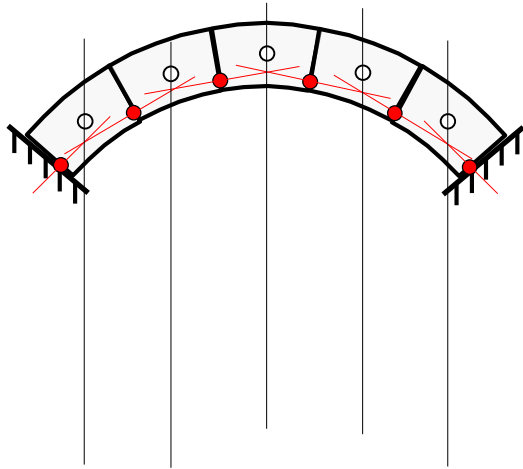
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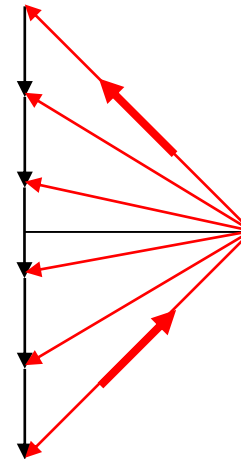
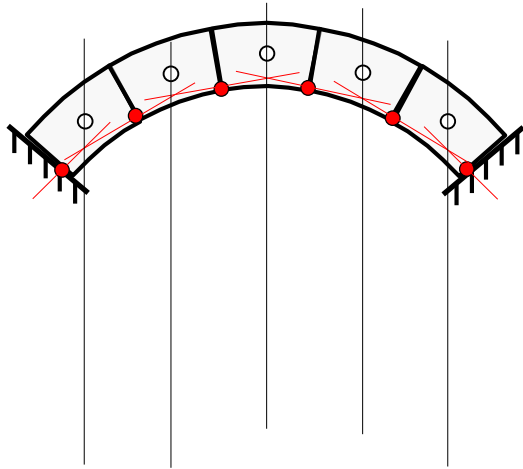
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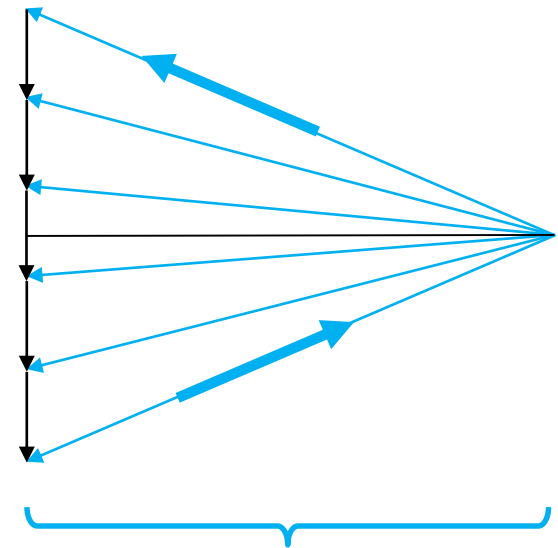
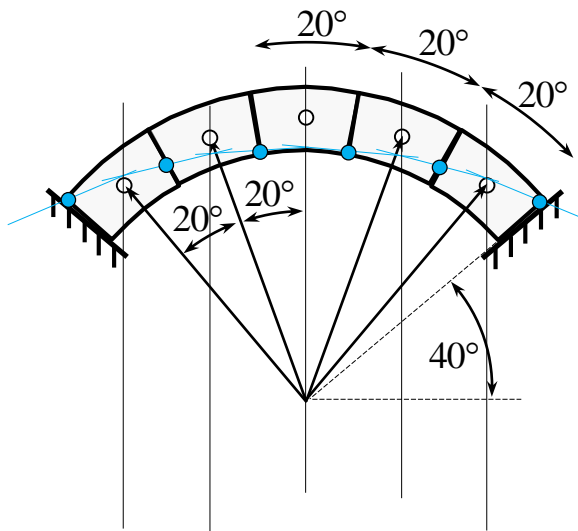
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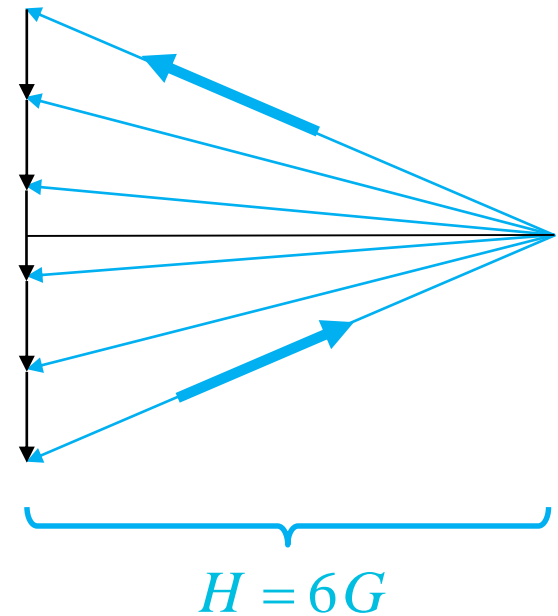
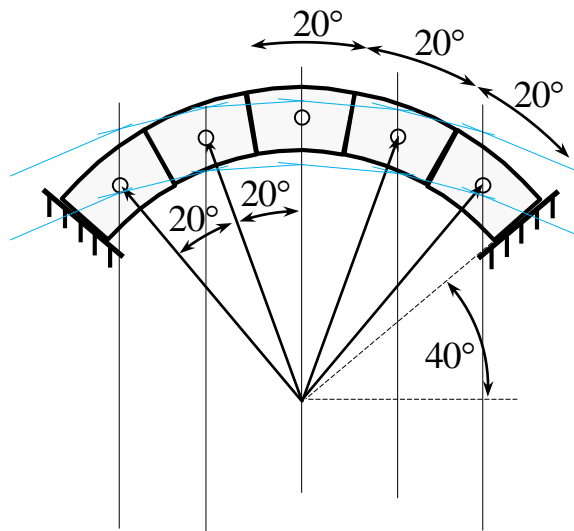
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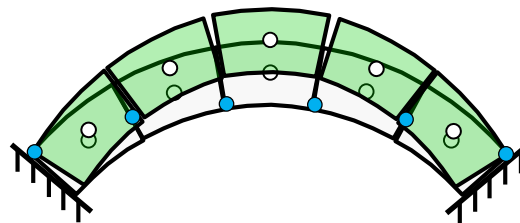
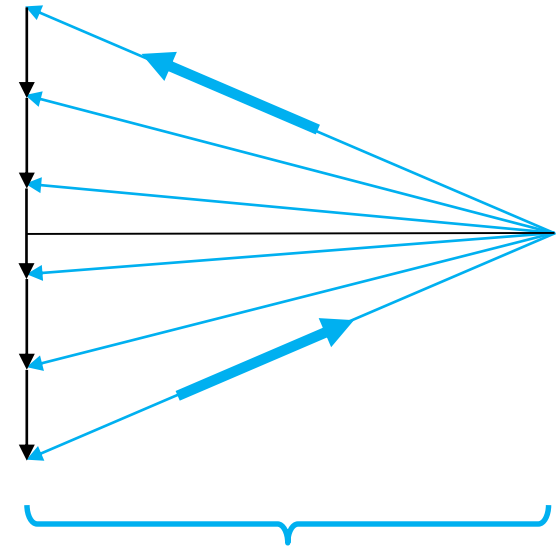
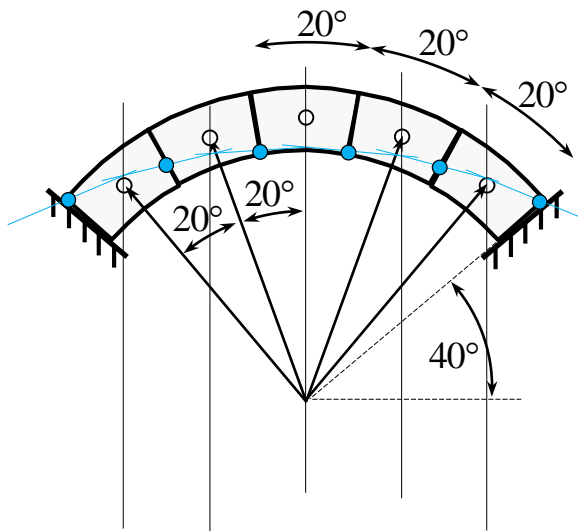
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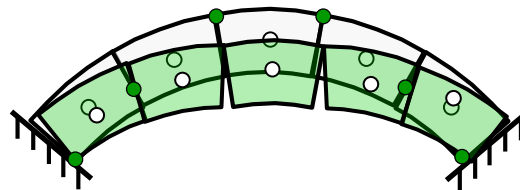
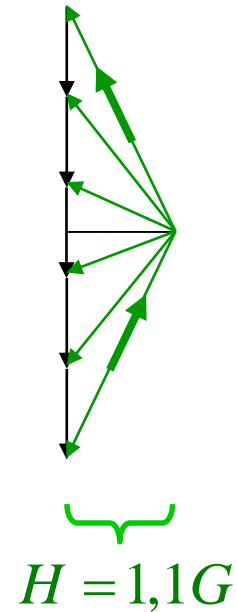
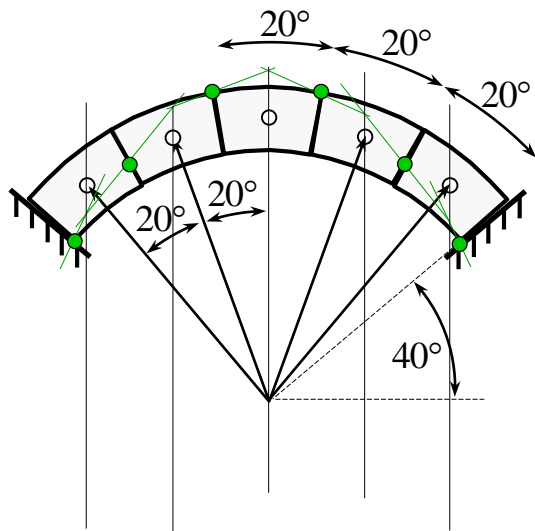
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Question: arch submitted to its selfweight; ?reactions? ?contact forces?



# The basic problem: Stability of an arch

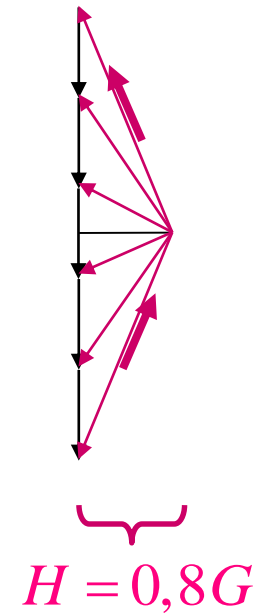
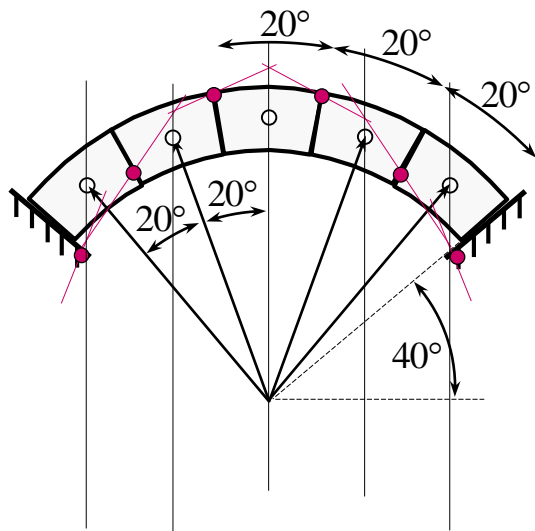
Question: arch submitted to its selfweight; ?reactions? ?contact forces?



a wide range of equilibrium solutions:  $\Leftarrow$  because the arch is thick enough !

# The basic problem: Stability of an arch

Question: arch submitted to its selfweight; ?reactions? ?contact forces?



**EQUILIBRIUM IS IMPOSSIBLE WITH THIS  $H$**

$\Rightarrow$  possible direction of the reactions is limited

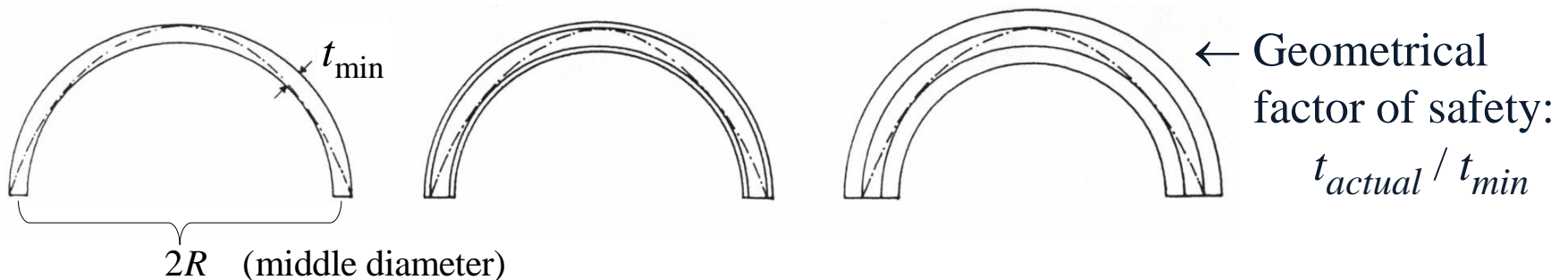
# The basic problem: Stability of an arch

Question: arch submitted to its selfweight; ?reactions? ?contact forces ?

Solution for an arch having *infinitely dense, radially oriented* contacts, with *zero tension resistance* ?  $\Rightarrow$  thrust line must run inside the arch

Ideal shape of the arch to produce thrust line through the contacts centroids:  
ch-curve („chain curve”)

Existing arches: typically circular middle curve (or composed of circular arcs)



$t_{min}$ : smallest uniform thickness for which the arch can carry its selfweight

semicircle:

Heyman (1966):  $t_{min} = 0,1059 \cdot R$

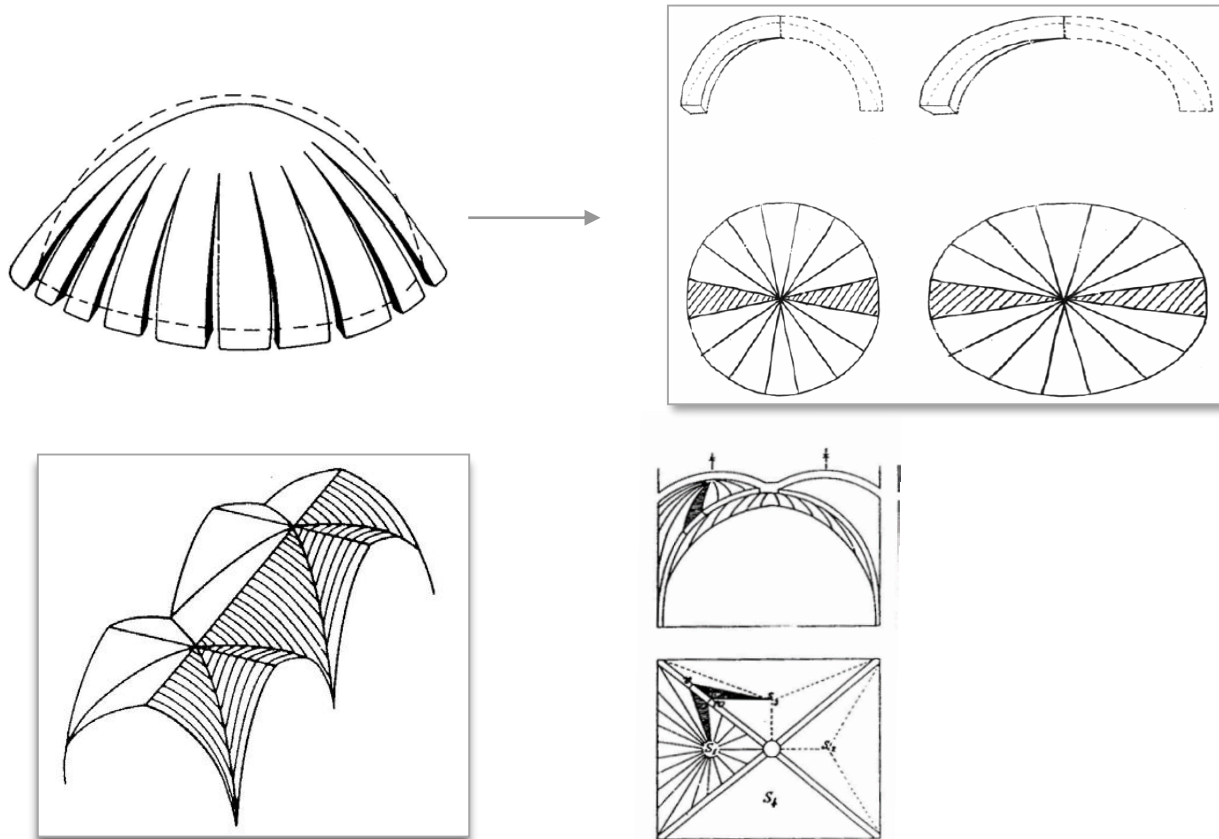
Milankovitch (1907):  $t_{min} = 0,1075 \cdot R$



# Stability of vaults under selfweight

Slicing technique: cut into individual arches, and check them separately!

XIXth century: different assumptions on the internal force system  
based on the inspection of typical crack patterns: e.g.



*pictures from: Huerta, 2001 and the references therein*

# Stability of vaults under selfweight

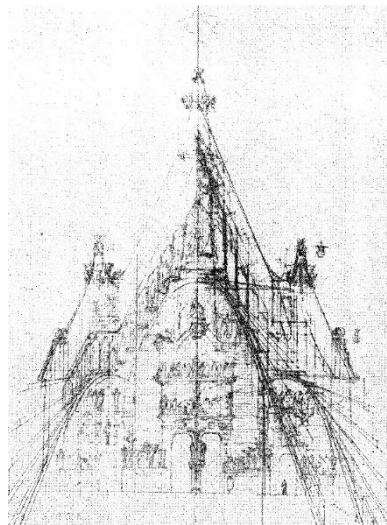
Slicing technique:

Gaudi, Sagrada Familia, Barcelona:

designed by:

→ graphical statics:

slice of the structure:

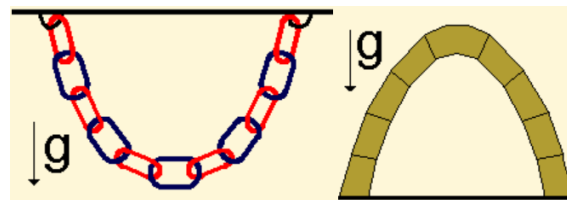


*Rafals, 1929*



*N. Valencia, archdaily.com*

→ physical models:



<http://www.art-nouveau-around-the-world.org/en/villes/barcelona/models.htm>



<http://dataphys.org/list/gaudis-hanging-chain-models/>

# Stability of vaults under selfweight

## Slicing technique:



<https://spainattractions.es/palma-cathedral-mallorca/>

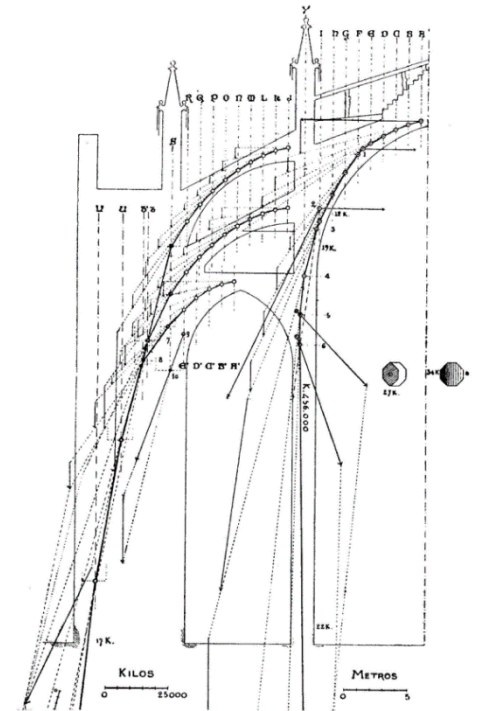
## Problem:

extremely tall slender pillars of the main nave

→ is it safe?

Rubio Bellver, 1912: graphical statics analysis

⇒ weights needed over the crown!



Rubio Bellver, 1912



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e.g. Vitruvius

e.g. Gothic rules

### Graphical statics

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Durand-Claye's stability area method for arches

computerized & extended for domes: Aita et al 2003 ... 2018

Wolfe's method for membrane forces in domes

O'Dwyer's funicular analysis  $\Rightarrow$

Thrust Network Analysis (TNA)

Questions

# Durand-Claye's stability area method

Durand-Claye, 1867: Symmetric arches & symmetric vertical loads

Admissible  $(P, e)$  pairs?

Consider a contact  $j$ ,

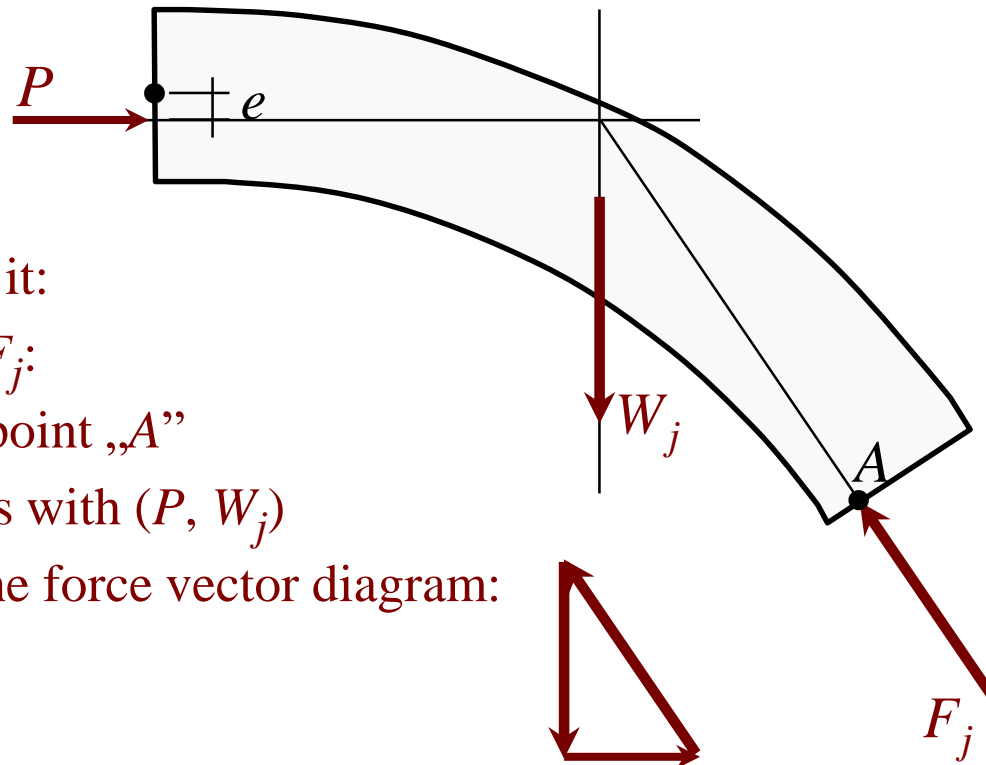
and a point „A” on it:

Contact force resultant,  $F_j$ :

acts at the chosen point „A”

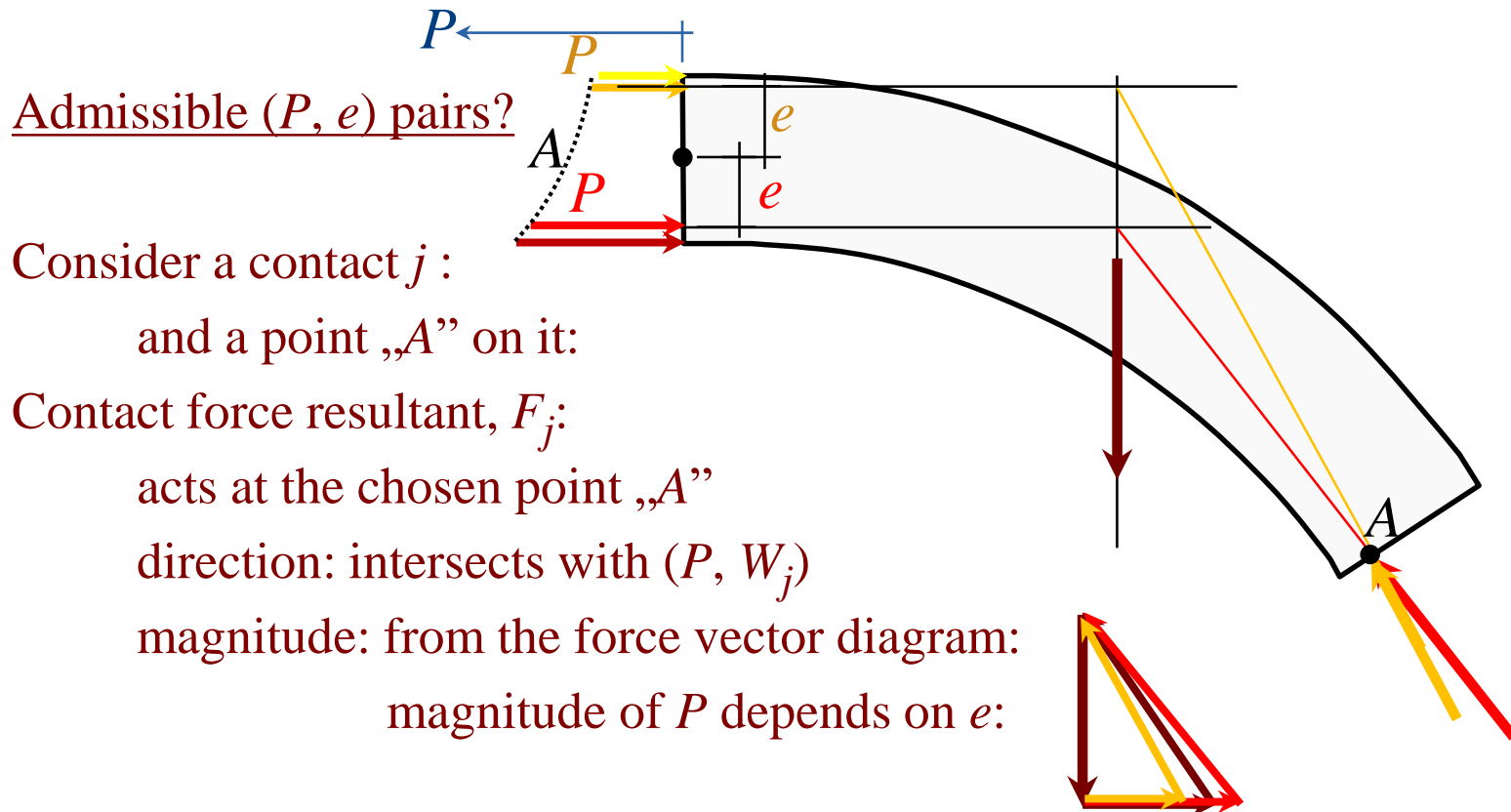
direction: intersects with  $(P, W_j)$

magnitude: from the force vector diagram:



# Durand-Claye's stability area method

Durand-Claye, 1867: Symmetric arches & symmetric vertical loads

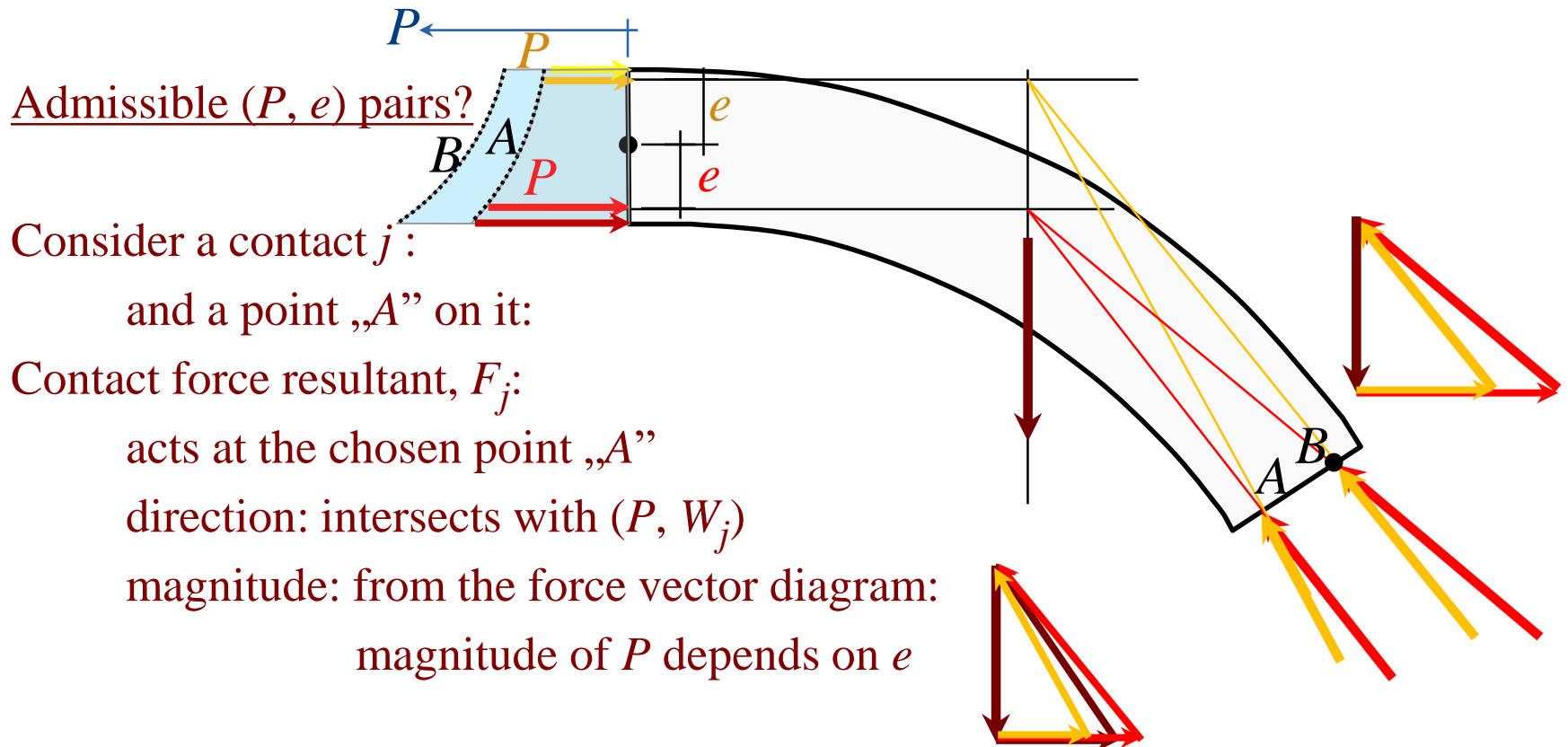


Possible magnitudes of  $P$  belonging to „A”:

[see dotted line above]

# Durand-Claye's stability area method

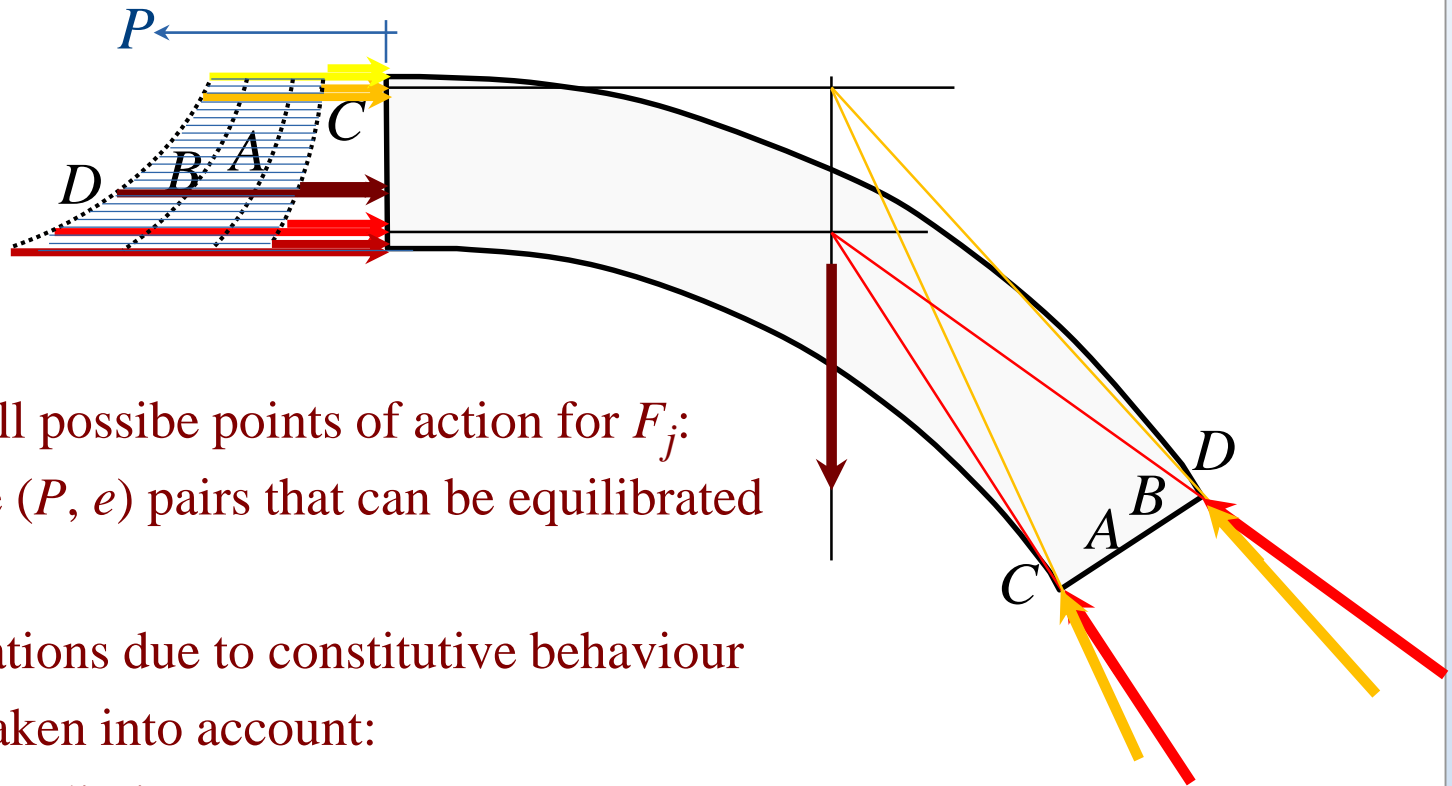
Durand-Claye, 1867: Symmetric arches & symmetric vertical loads



Possible magnitudes of  $P$  belonging to „A”: [see grey domain horizontal sizes]  
 similarly to any „B”: [see cyan domain horizontal sizes]

# Durand-Claye's stability area method

Durand-Claye, 1867: Symmetric arches & symmetric vertical loads



Considering all possible points of action for  $F_j$ :  
found those  $(P, e)$  pairs that can be equilibrated

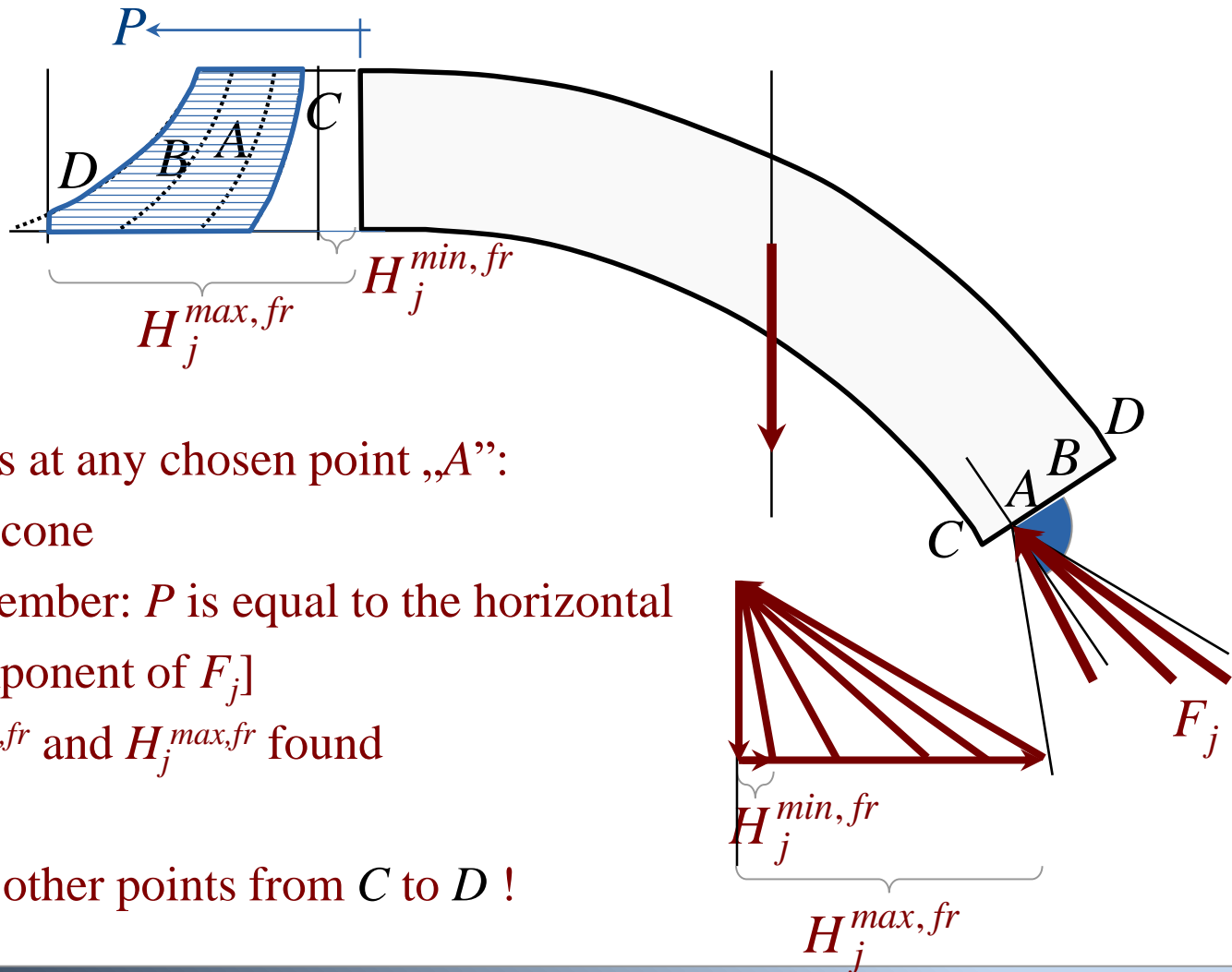
now the limitations due to constitutive behaviour  
have to be taken into account:

- friction limit
- compression strength
- [ in new versions: tension strength – will not be shown here ]



# Durand-Claye's stability area method

Durand-Claye, 1867: Symmetric arches & symmetric vertical loads



Friction limit:

if  $F_j$  acts at any chosen point „A”:

friction cone

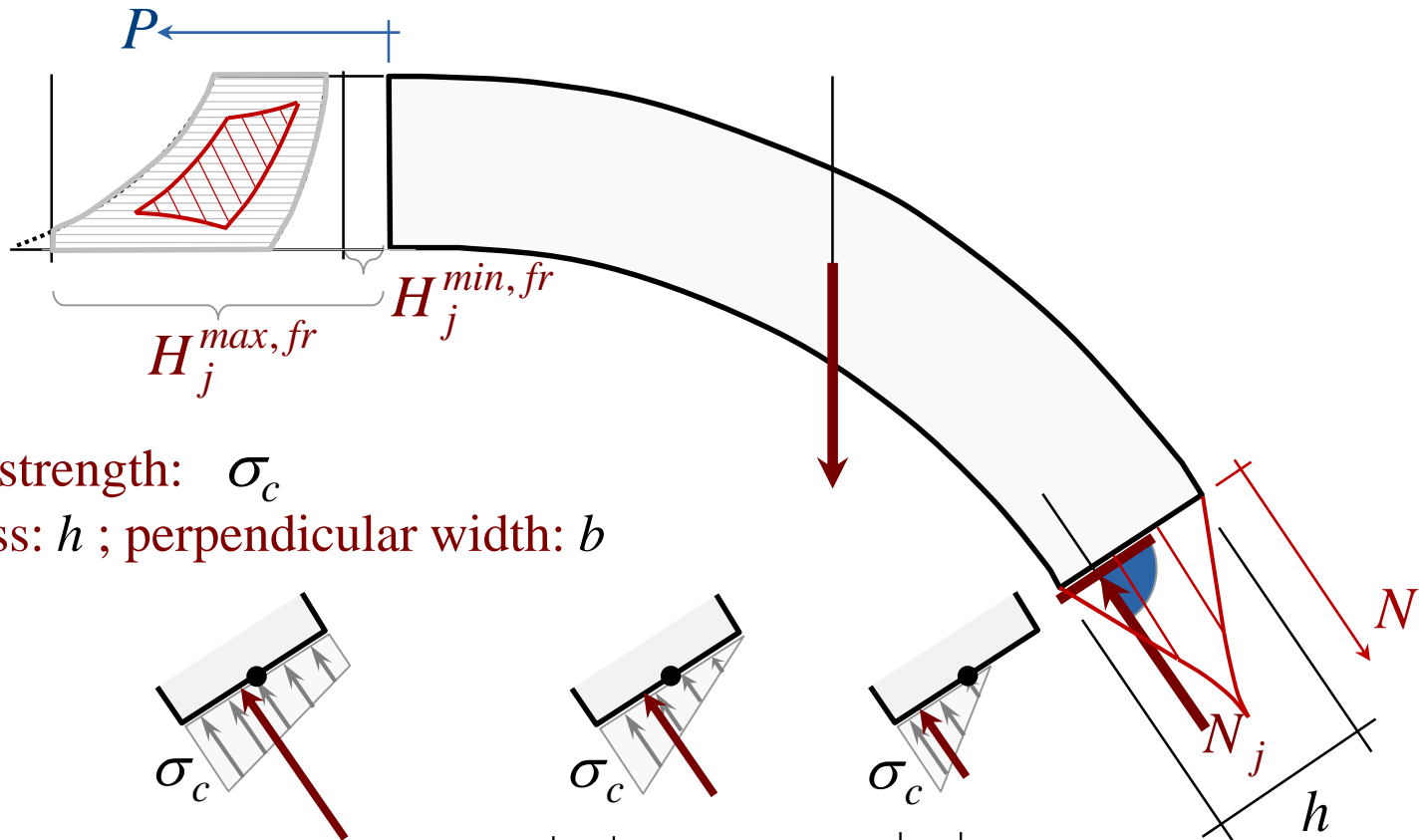
[remember:  $P$  is equal to the horizontal component of  $F_j$ ]

$\Rightarrow H_j^{min,fr}$  and  $H_j^{max,fr}$  found

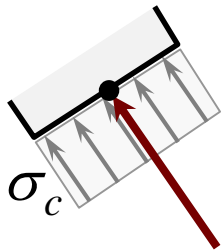
Equals for all other points from  $C$  to  $D$  !

# Durand-Claye's stability area method

Durand-Claye, 1867: Symmetric arches & symmetric vertical loads

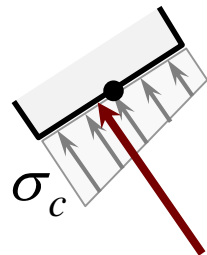


Compression strength:  $\sigma_c$   
 thickness:  $h$  ; perpendicular width:  $b$



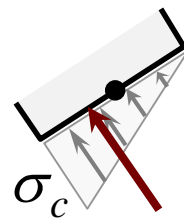
$$e_N = 0:$$

$$N \leq b \cdot h \cdot \sigma_c$$



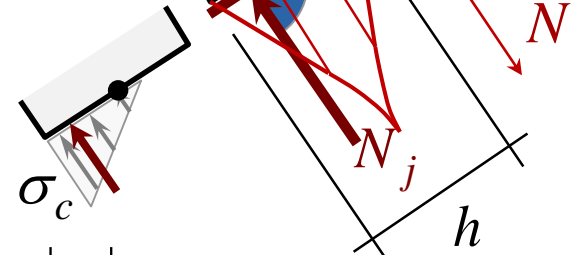
$$|e_N| \leq h/6:$$

$$N \leq \frac{h}{h + 6 \cdot |e_N|} \cdot b \cdot h \cdot \sigma_c$$



$$|e_N| = h/6:$$

$$N \leq \frac{1}{2} b \cdot h \cdot \sigma_c$$

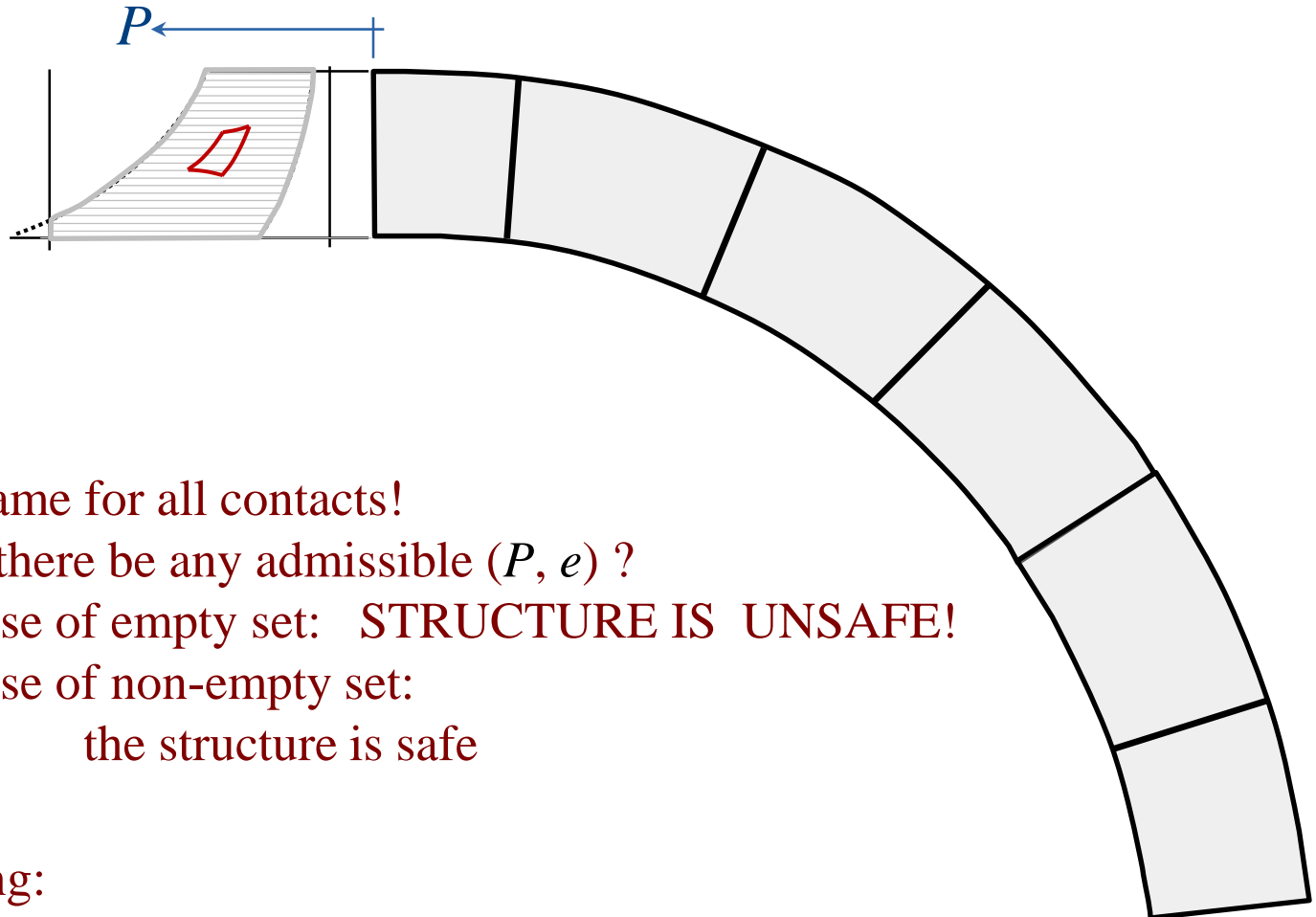


$$|e_N| \geq h/6:$$

$$N \leq \frac{3}{2} \left( \frac{h}{2} - |e_N| \right) \cdot b \cdot \sigma_c$$

# Durand-Claye's stability area method

Durand-Claye, 1867: Symmetric arches & symmetric vertical loads



Now do the same for all contacts!

→ will there be any admissible  $(P, e)$  ?

In case of empty set: **STRUCTURE IS UNSAFE!**

In case of non-empty set:

the structure is safe

Further reading:

Foce & Aita (2003); Aita et al (2017)

# Durand-Claye's stability area method

## Applications:

e.g. Barsotti et al (2017):

comparison of different arch types

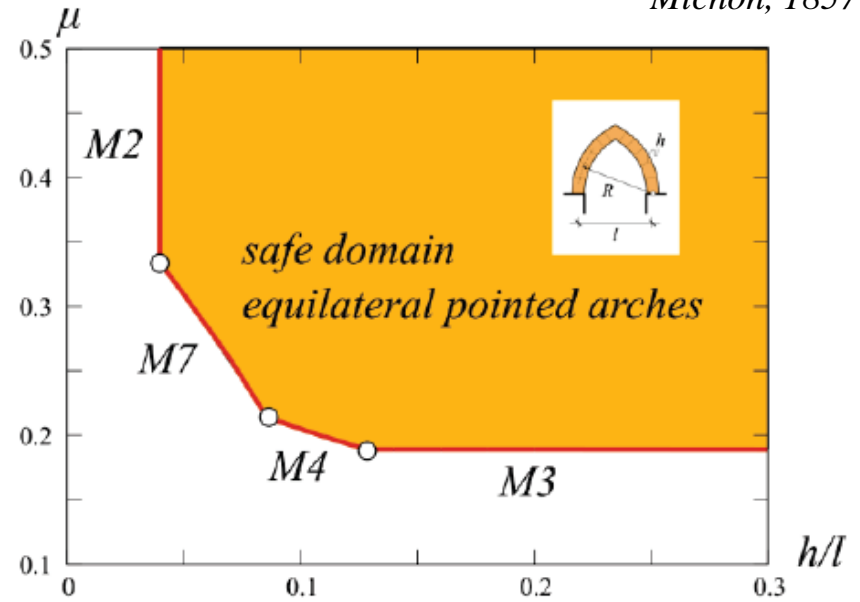
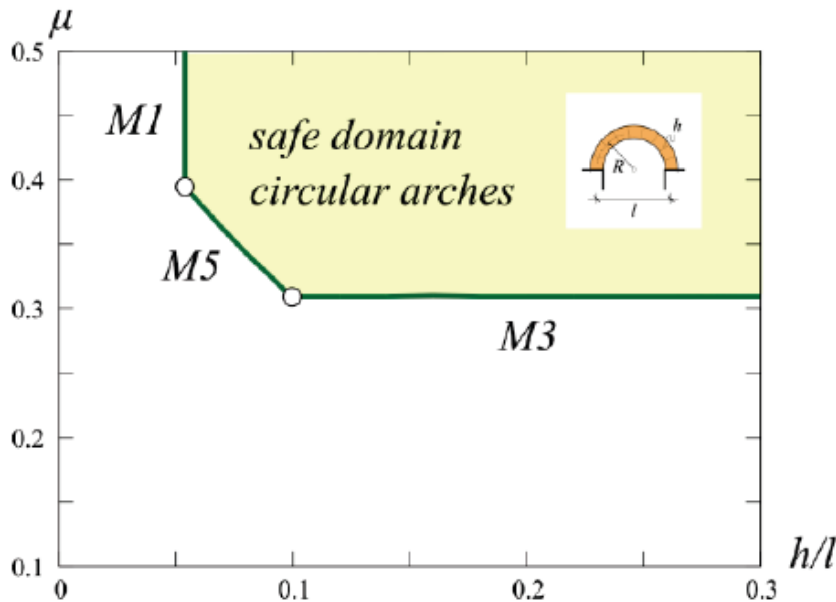
and their possible collapse modes

$\mu$  : friction coefficient

$h$  : arch thickness;  $l$  : span



Michon, 1857



# Durand-Claye's stability area method

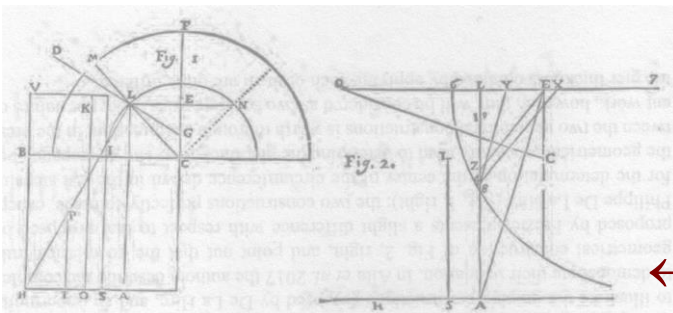
## Applications:

e.g. Aita et al (2018a):

geometrical factor of safety for historic design rules:

- find necessary minimum value of a certain size with Durand-Claye's;
- find that size according to historic rule;
- compare!

Comparison of different historical rules for pier thickness  
for the same arch-wall-pier system:

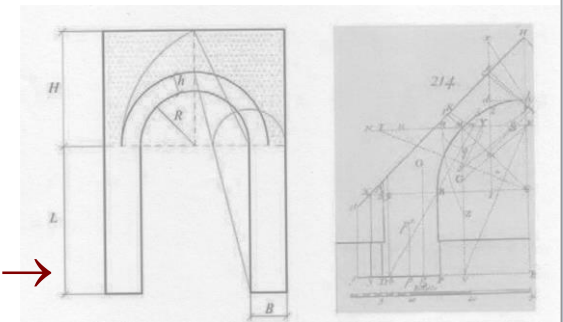


*La Hire, 1731*

limit width according  
to the Durand-Claye's  
method: 2,54 m

← 2,81 m

3,61 m →



*Frézier, 1737*

# Durand-Claye's stability area method

## Applications:

e.g. Aita et al (2018b): Safety assessment of the dome of Pisa Cathedral



*tripadvisor.co.za*

constructed: XIth century  
dome: oval groundplan,  
≈ circular meridians



restoration of the dome going on recently

„On the north side... at about eye level, is an original piece of Roman marble, on which are a series of small black marks. Legend says that these marks were left by the Devil when he climbed up to the dome attempting to stop its construction, and so they are referred to as the scratches of the devil. The legend also says that out of spite the number of scratches always changes when counted.” (Wikipedia)

# Durand-Claye's stability area method

## Applications:

e.g. Aita et al (2018b):

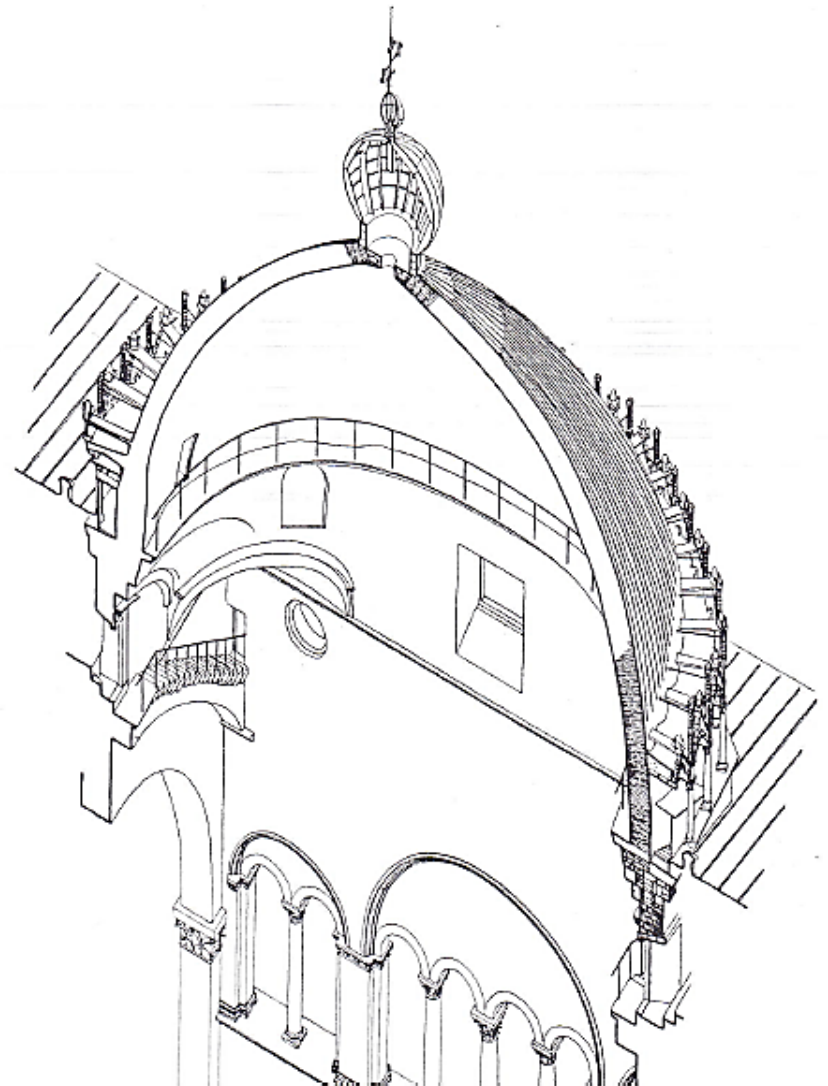
- D-C method extended for domes  
with membrane forces  
(Durand-Claye, 1880)
- analysis of the dome

## Result:

geometrical factor of safety  $\approx 2$

## Further reading:

Aita (2018b)



# THIS LECTURE:

## GRAPHICAL METHODS

Historical times: Practical geometrical rules

e.g. Vitruvius

e.g. Gothic rules

### Graphical statics

The basic problem: Stability of an arch

Durand-Claye's stability area method for arches

computerized & extended for domes: Aita et al 2003 ... 2018

Wolfe's method for membrane forces in domes

O'Dwyer's funicular analysis  $\Rightarrow$

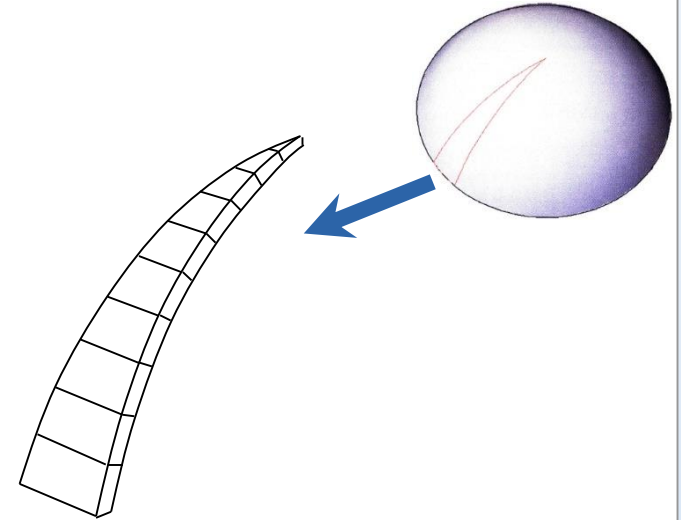
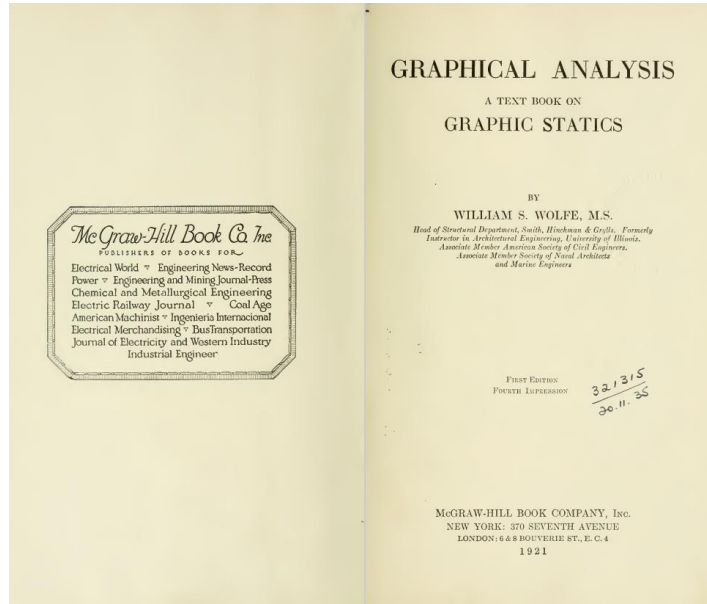
Thrust Network Analysis (TNA)

Questions



# Wolfe's method

Wolfe (1921);



→ Version 1.: domes with tension resistance

→ Version 2.: domes without tension resistance

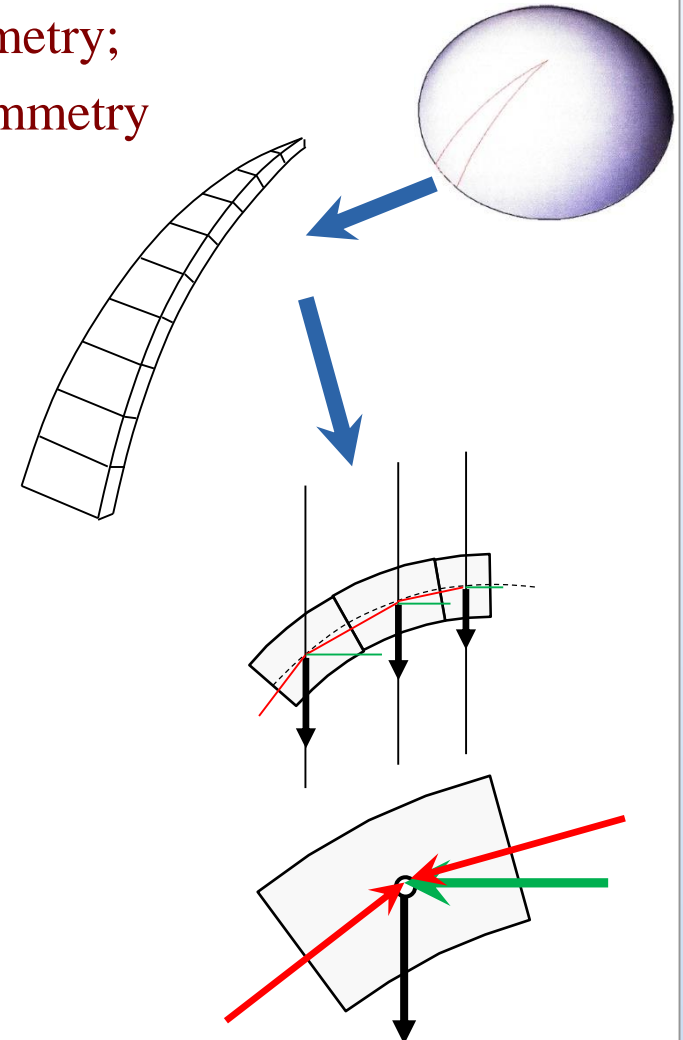
# Wolfe's method

- Restricted to: domes with *vertical axis* of symmetry;  
under *vertical loads* with vertical axis of symmetry
- basic assumption: *membrane state*

- Version 1.: domes with tension resistance
- Version 2.: domes without tension resistance

Starting step:  
weights of lune voussoirs; at centroids

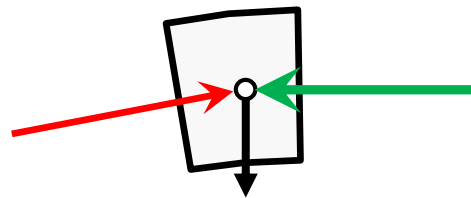
Assumption:  
contact force: line of action joins the two neighbouring centroids



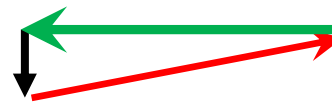
# Wolfe's method

- Restricted to: domes with *vertical axis* of symmetry;  
under *vertical loads* with vertical axis of symmetry
- basic assumption: *membrane state*

## 1. Analysis of the top segment:

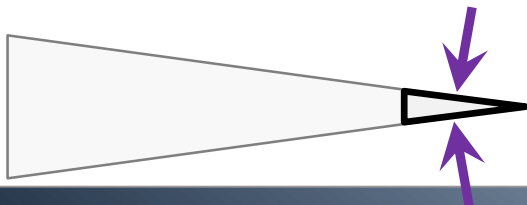


*funicular diagram*

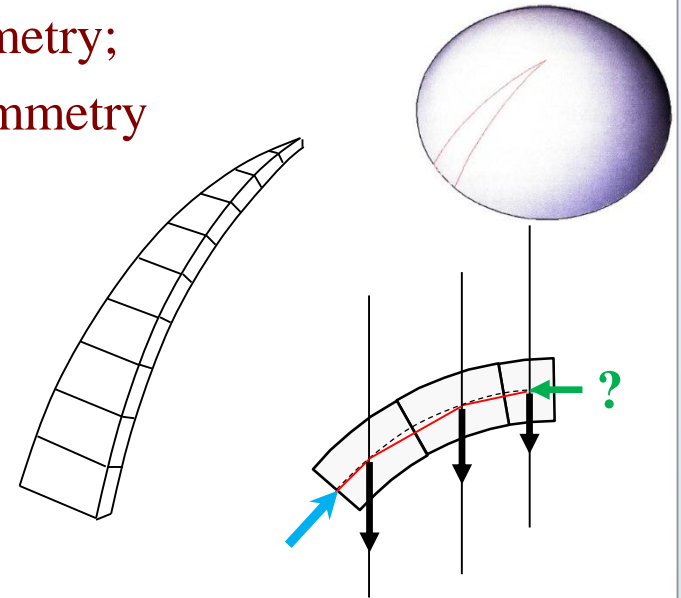


*force diagram, front view*

*top view:*



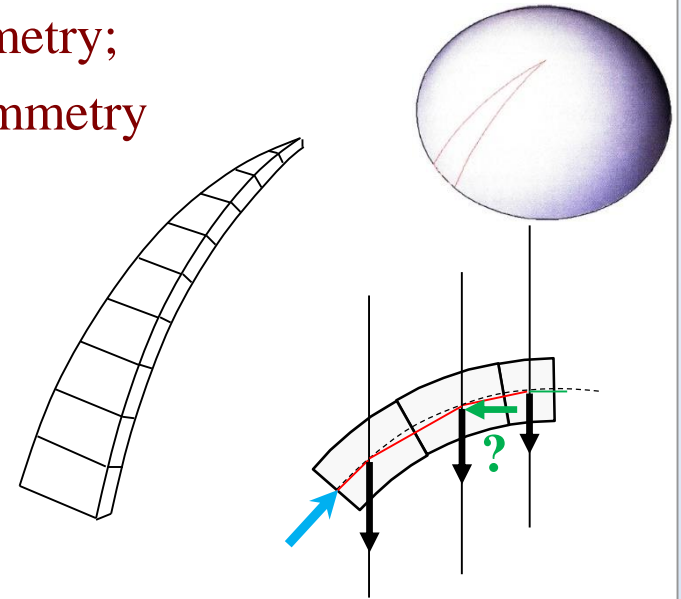
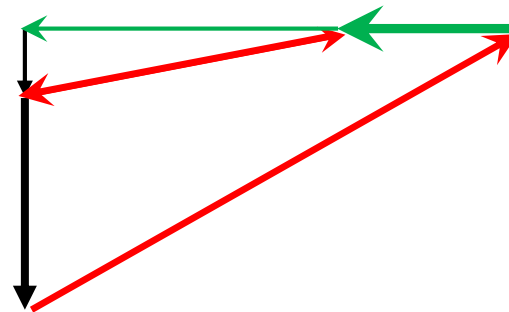
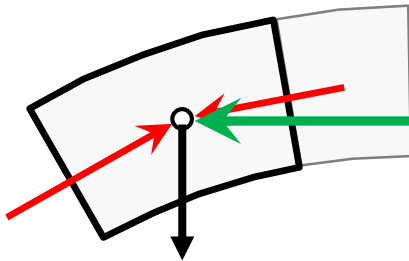
[ later ]



# Wolfe's method

- Restricted to: domes with *vertical axis* of symmetry;  
under *vertical loads* with vertical axis of symmetry
- basic assumption: *membrane state*  
⇒ contact force intersect with weight  
along the *middle line*

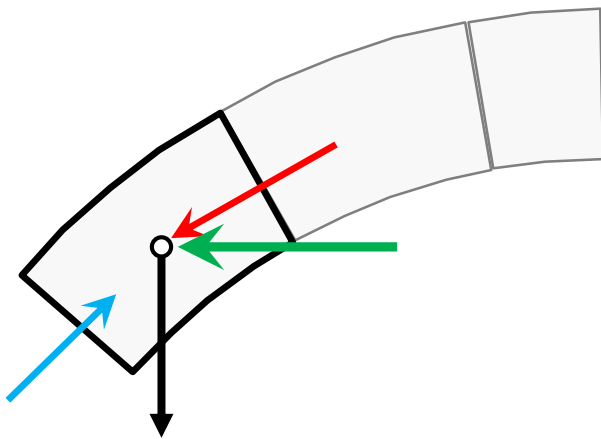
## 2. Analysis of the 2nd segment:



# Wolfe's method

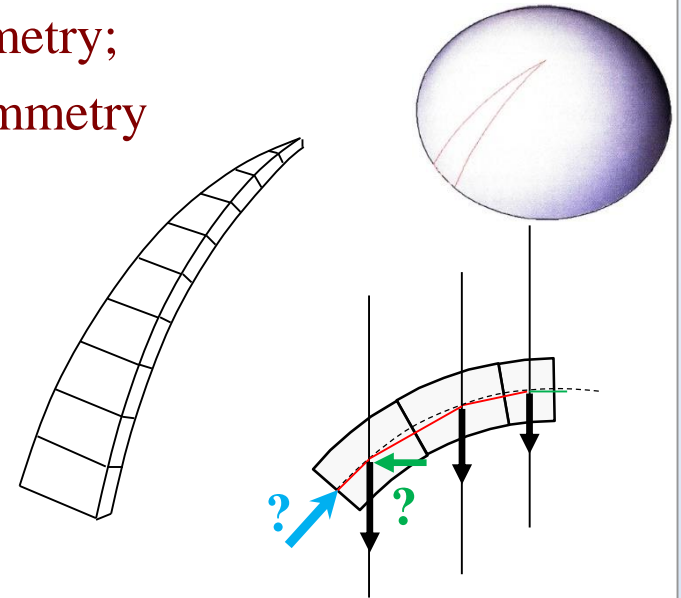
- Restricted to: domes with *vertical axis* of symmetry;  
under *vertical loads* with vertical axis of symmetry
- basic assumption: *membrane state*  
⇒ contact force intersect with weight  
along the *middle line*

## 3. Analysis of the bottom segment:



Assumption:

Reaction goes through the centroid of the last segment,  
perpendicular to lowest contact ( $\perp$  to the radial direction)

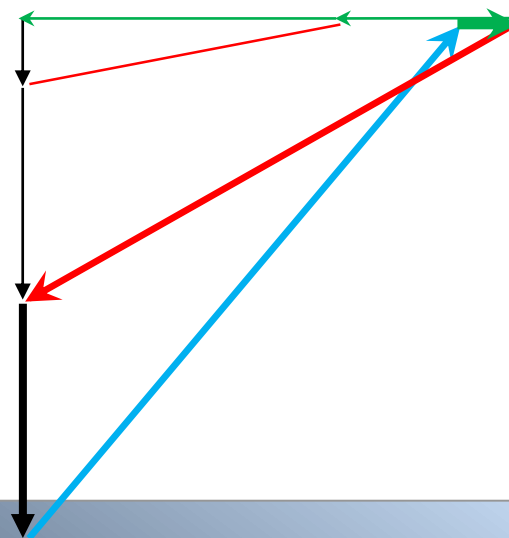
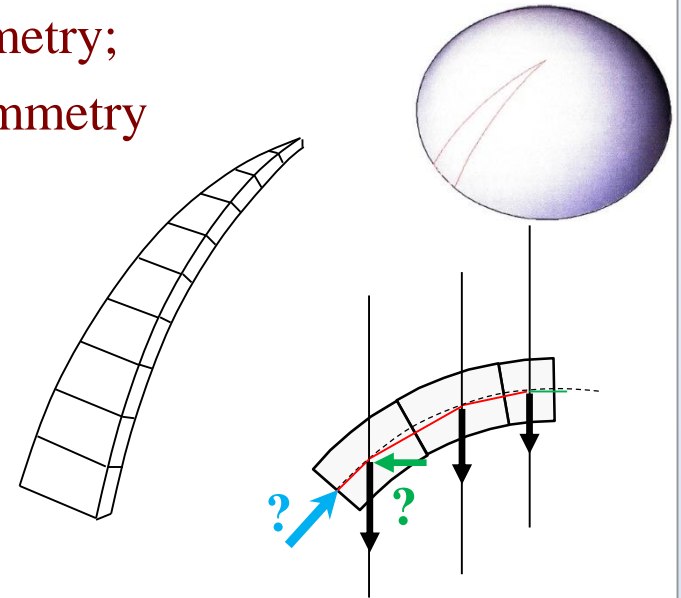
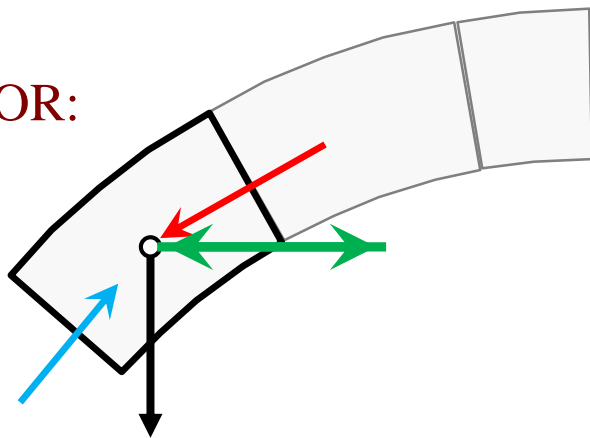


# Wolfe's method

- Restricted to: domes with *vertical axis* of symmetry;  
under *vertical loads* with vertical axis of symmetry
- basic assumption: *membrane state*  
⇒ contact force intersect with weight  
along the *middle line*

## 3. Analysis of the bottom segment:

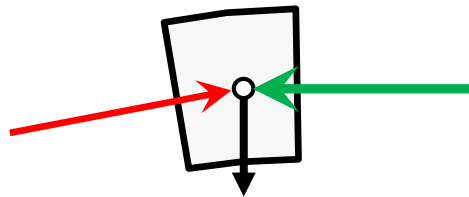
OR:



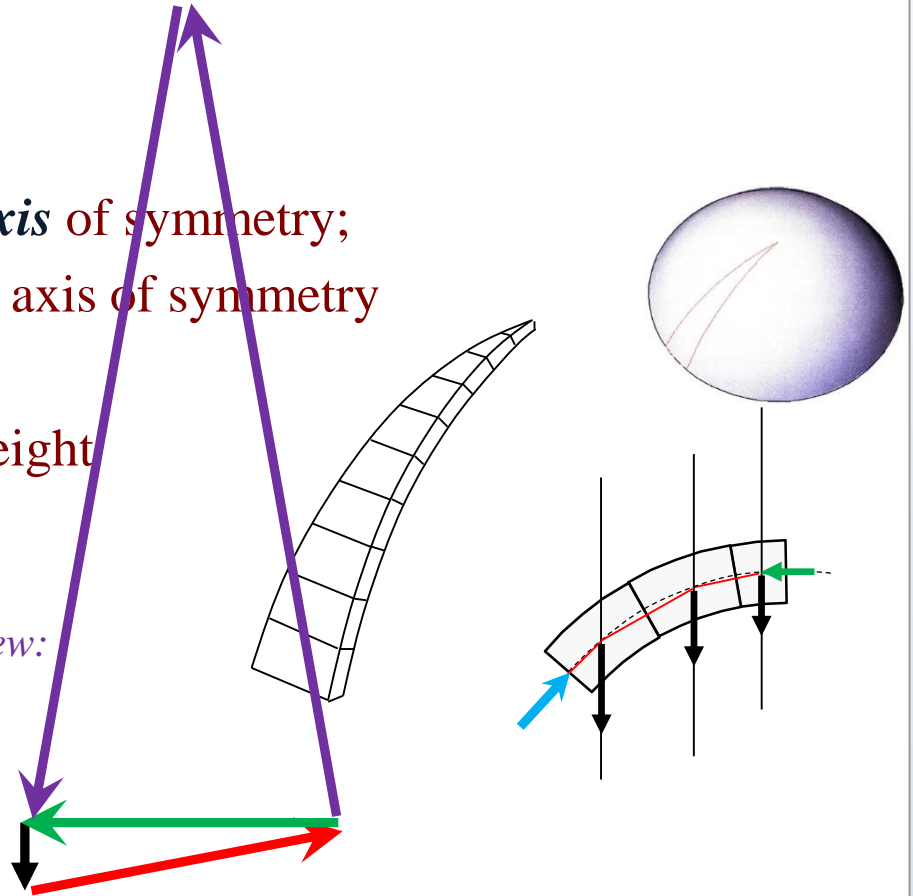
# Wolfe's method

- Restricted to: domes with *vertical axis* of symmetry;  
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- basic assumption: *membrane state*  
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along the *middle line*

## 1. Analysis of the top segment:

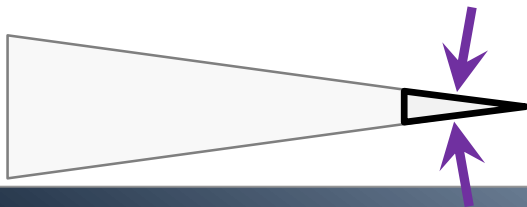


*top view:*



Hoop forces:

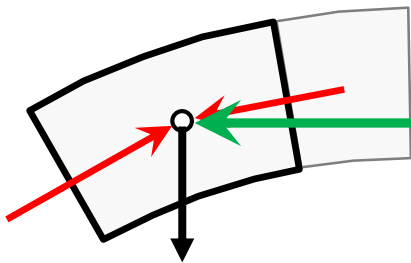
*top view:*



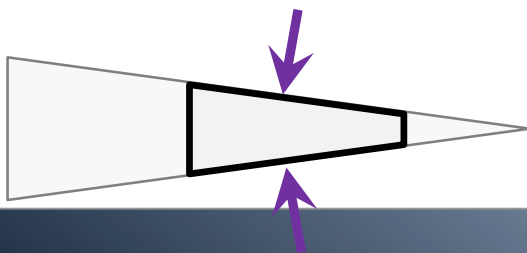
# Wolfe's method

- Restricted to: domes with *vertical axis* of symmetry;  
under *vertical loads* with vertical axis of symmetry
- basic assumption: *membrane state*  
⇒ contact force intersect with weight  
along the *middle line*

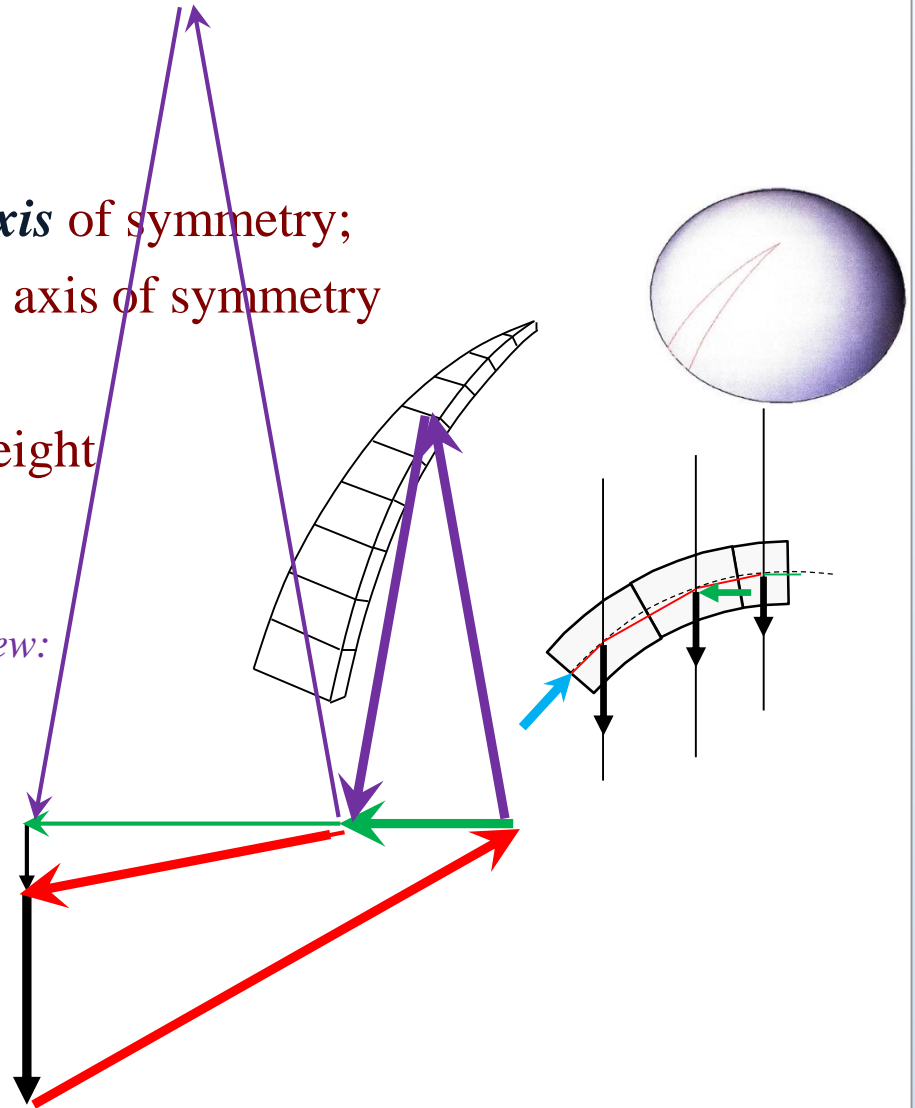
## 2. Analysis of the 2nd segment:



top view:



top view:





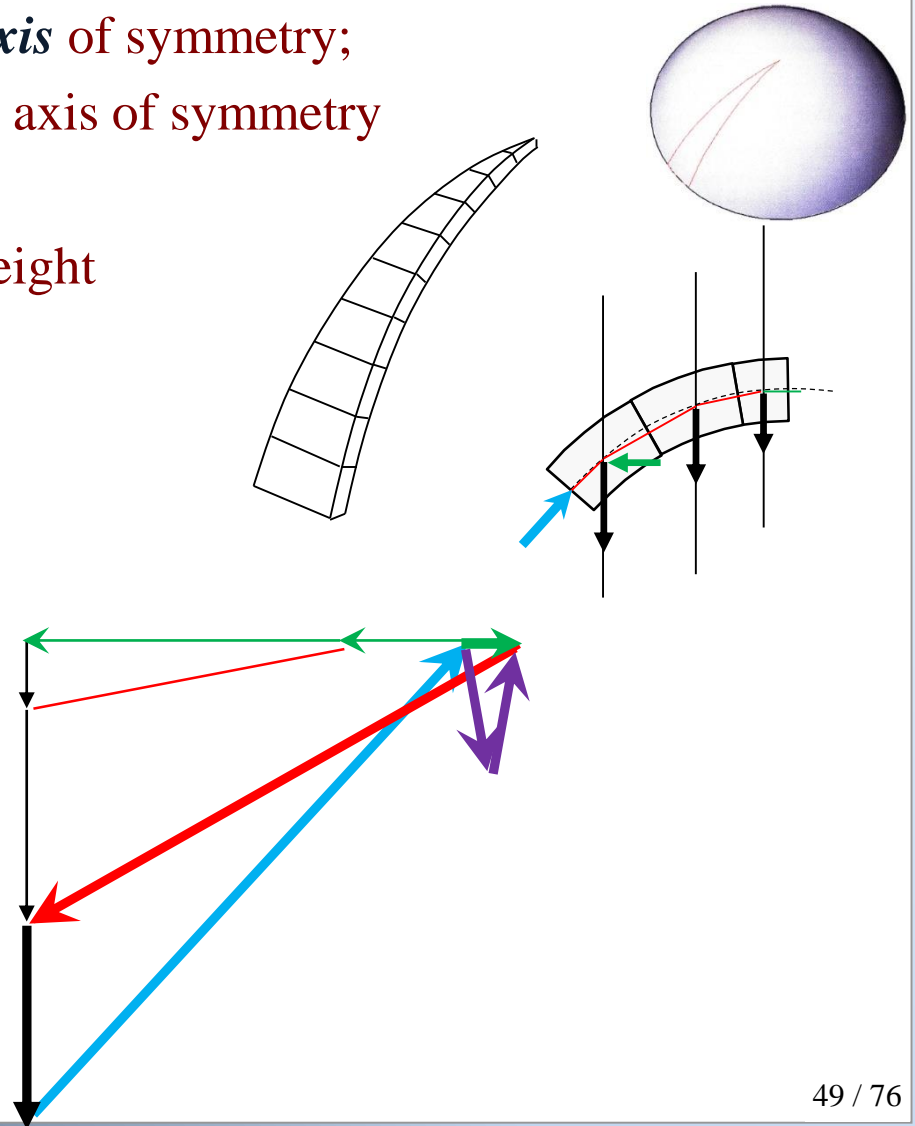
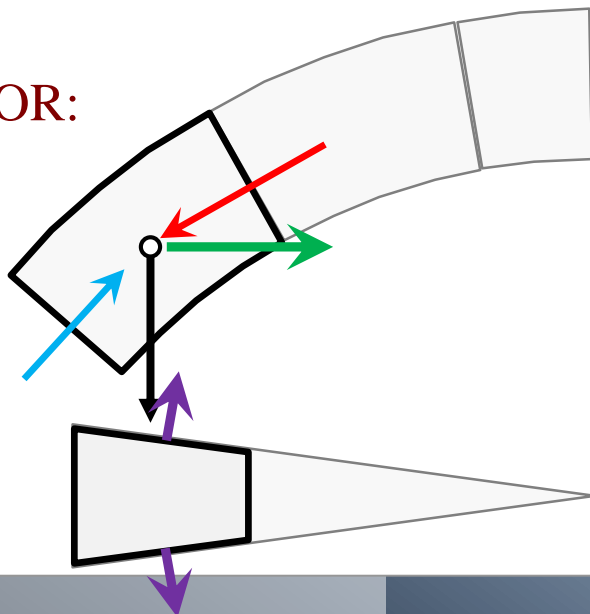


# Wolfe's method

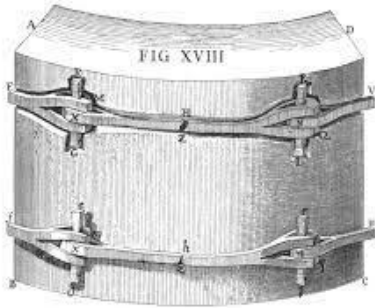
- Restricted to: domes with *vertical axis* of symmetry;  
under *vertical loads* with vertical axis of symmetry
- basic assumption: *membrane state*  
⇒ contact force intersect with weight  
along the *middle line*

## 3. Analysis of the bottom segment:

OR:



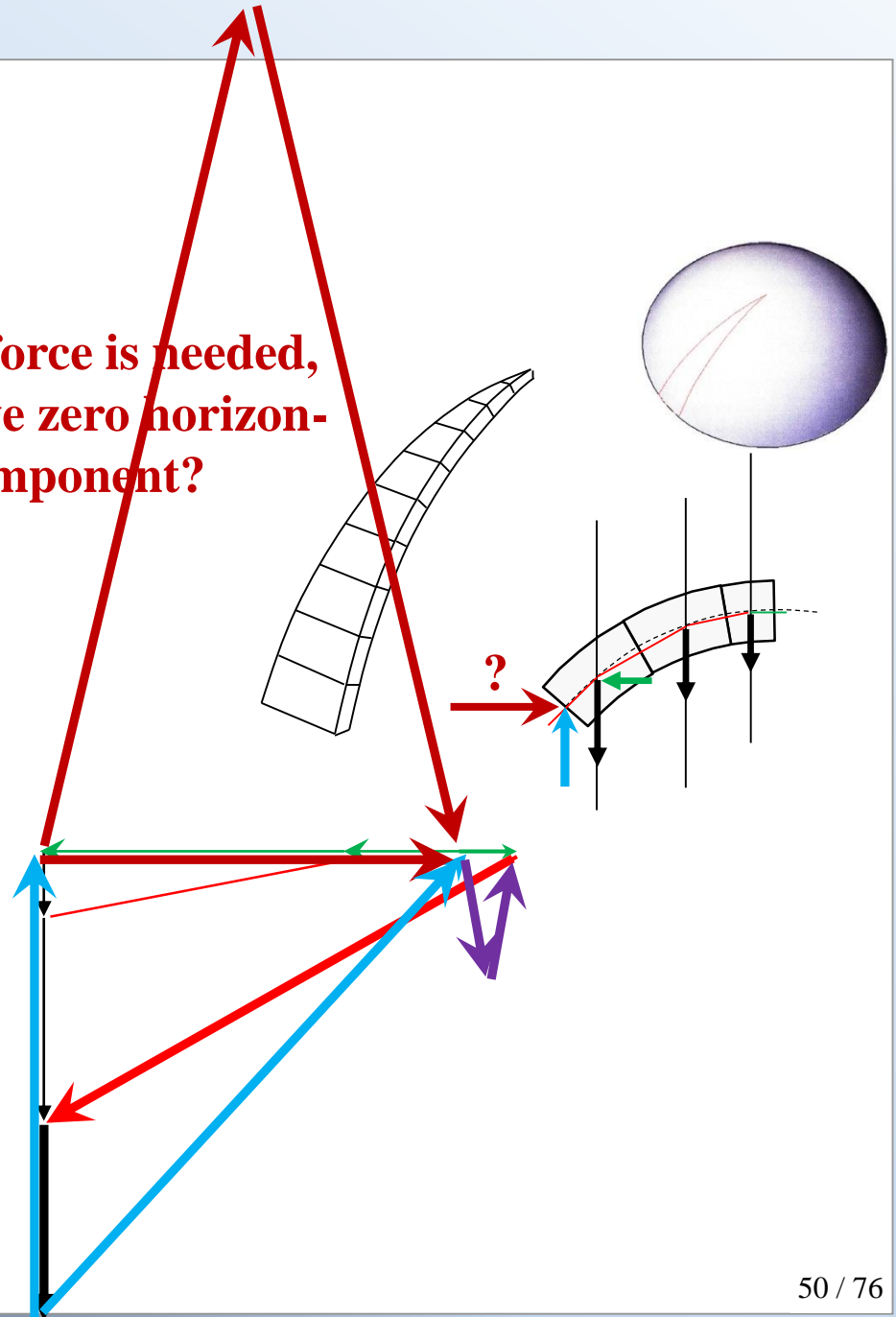
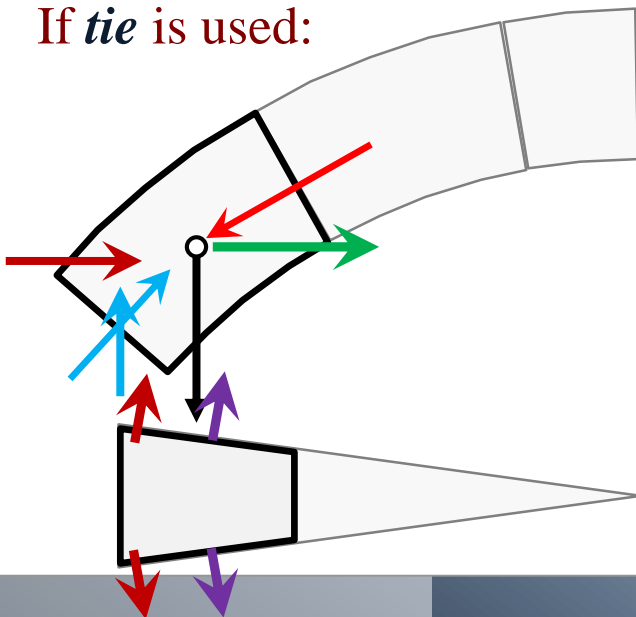
# Wolfe's method



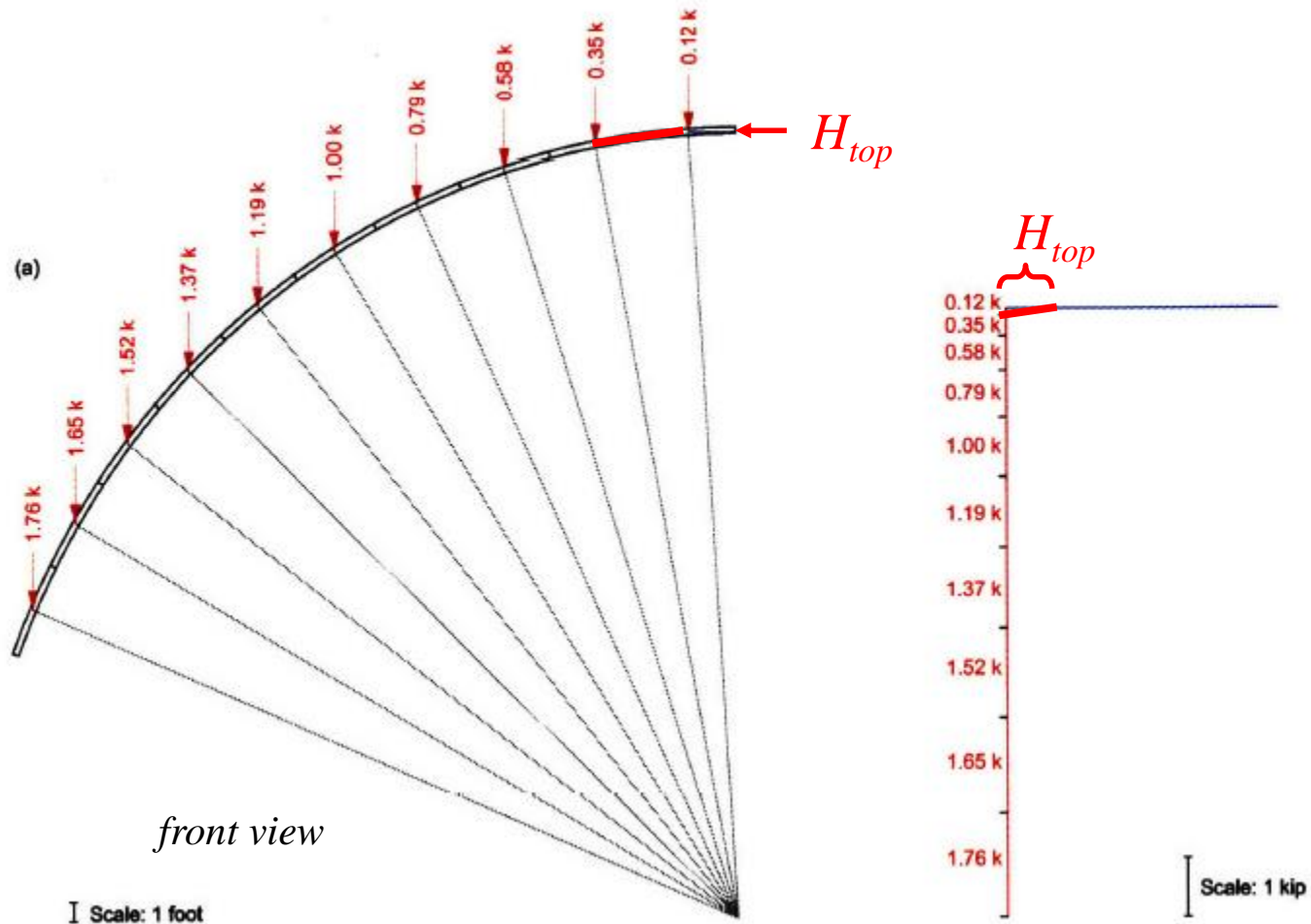
How large tie force is needed, in order to have zero horizontal reaction component?

## 3. Analysis of the 3rd segment:

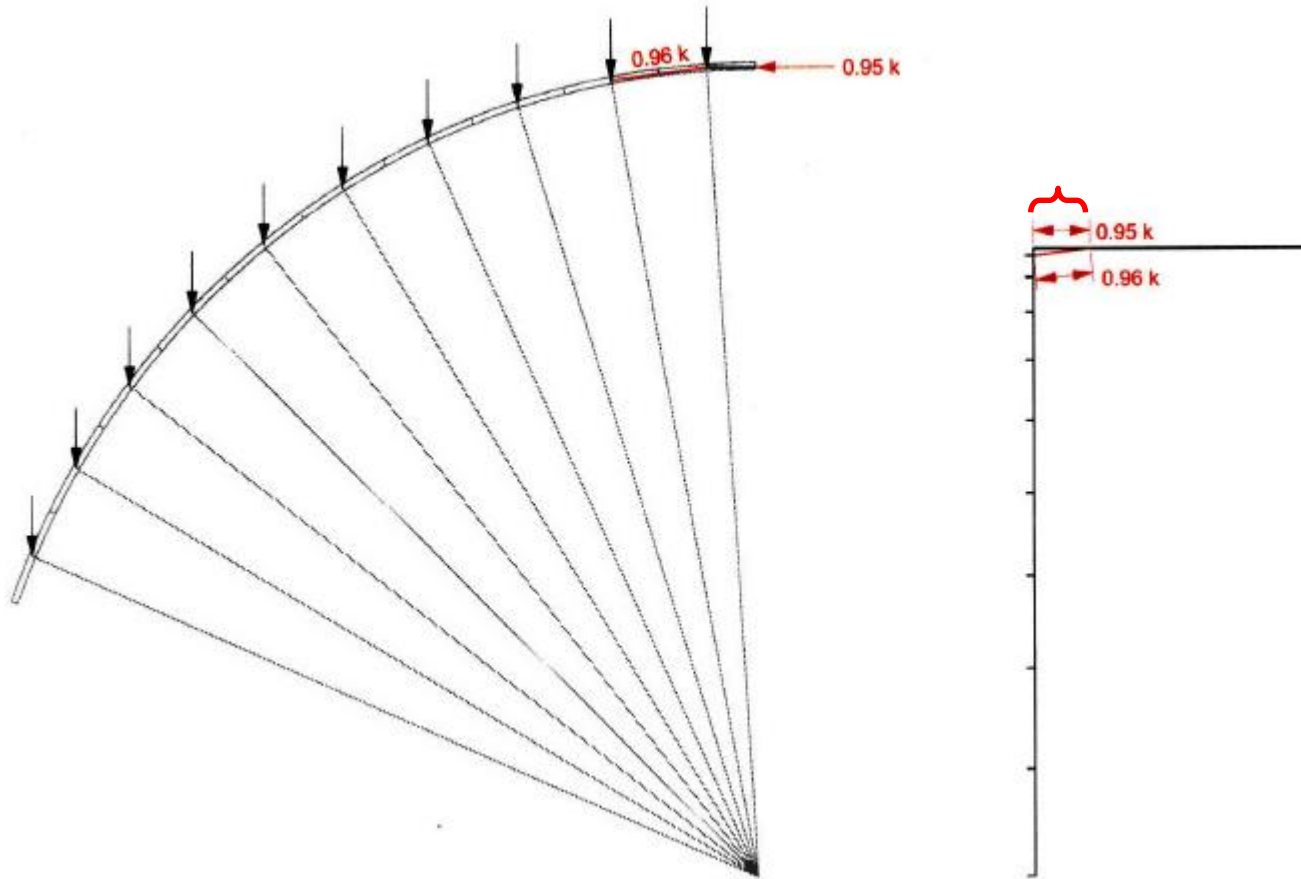
If *tie* is used:



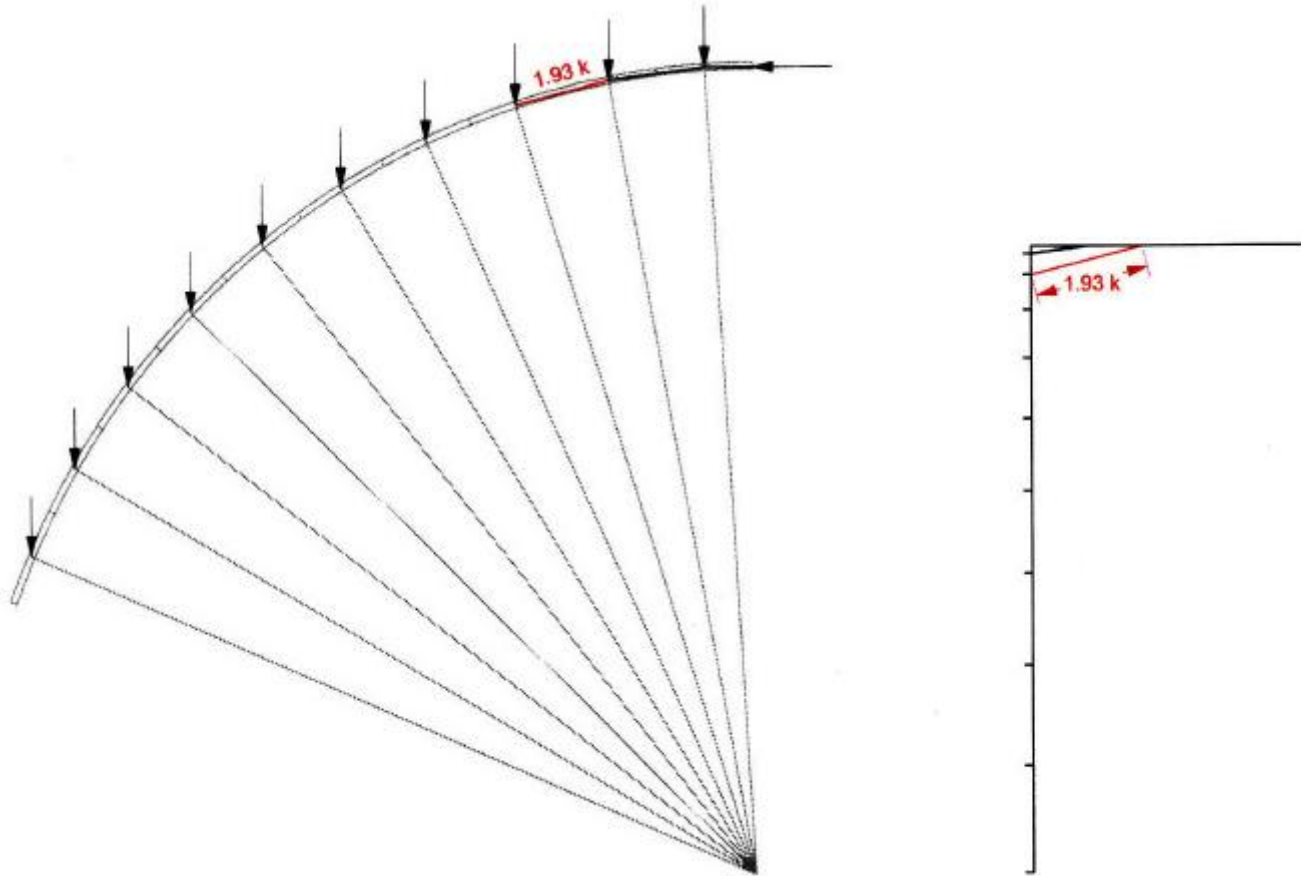
# Wolfe's method, for tension-resisting domes



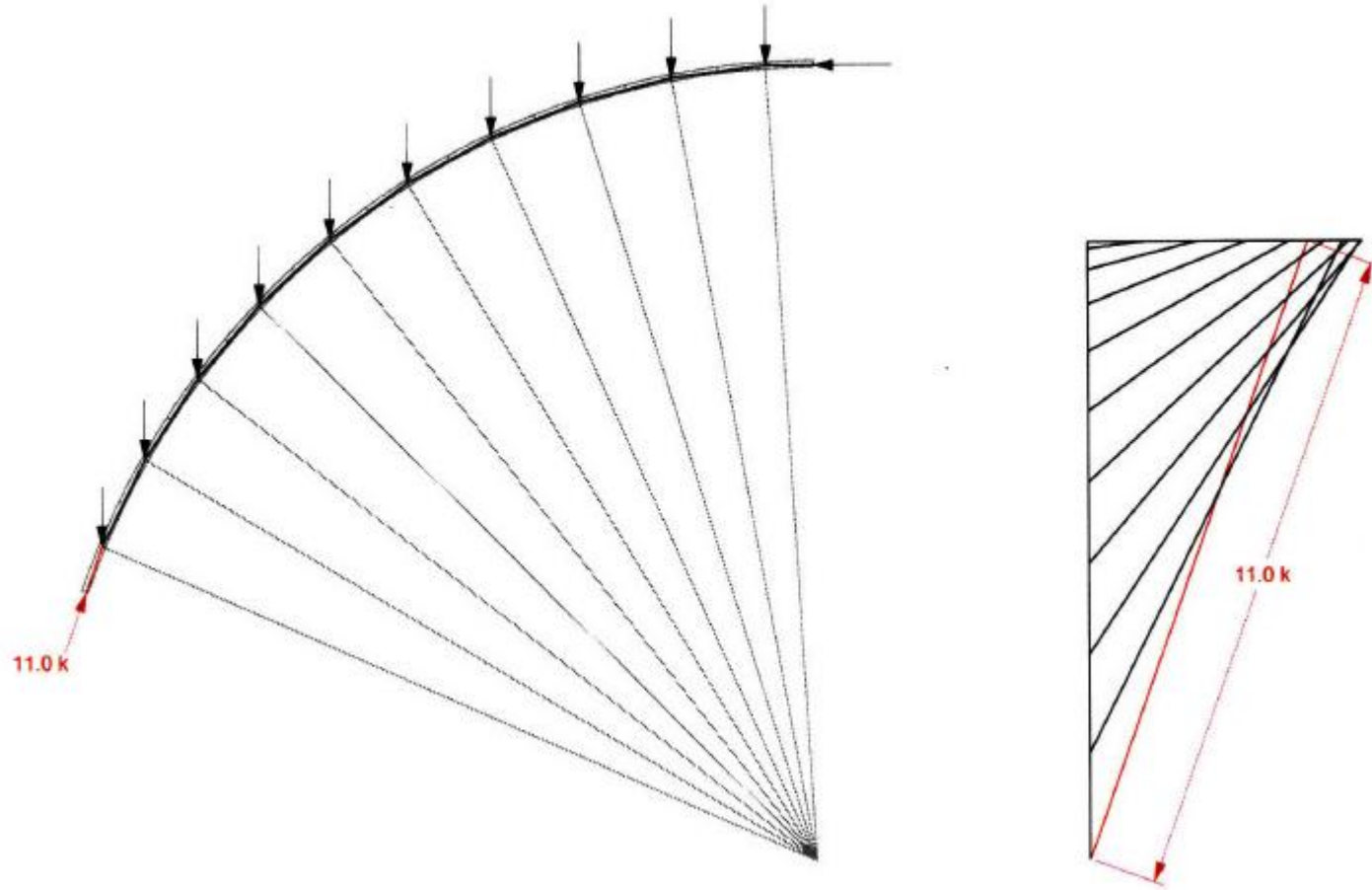
# Wolfe's method, for tension-resisting domes



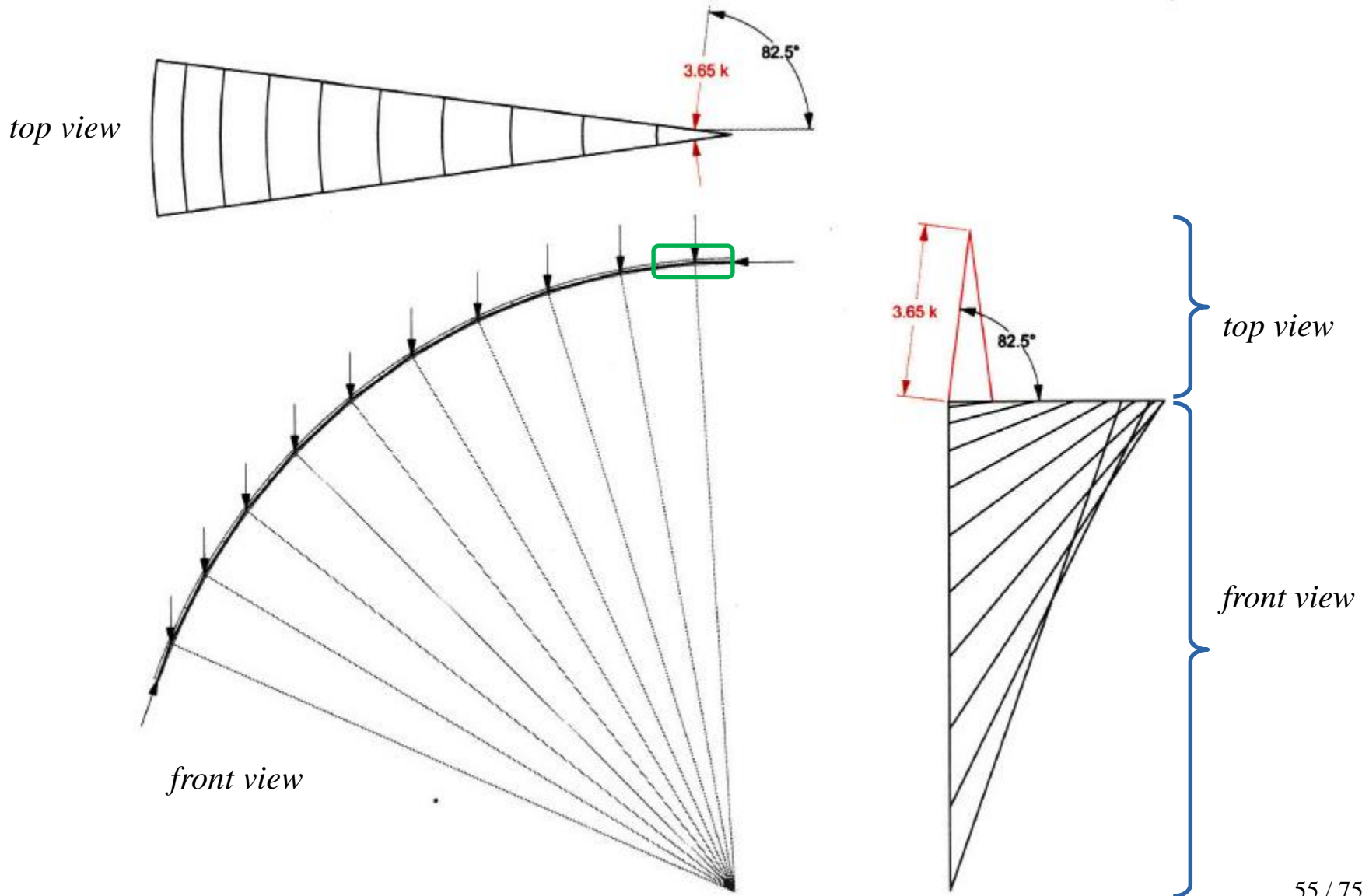
# Wolfe's method, for tension-resisting domes



# Wolfe's method, for tension-resisting domes

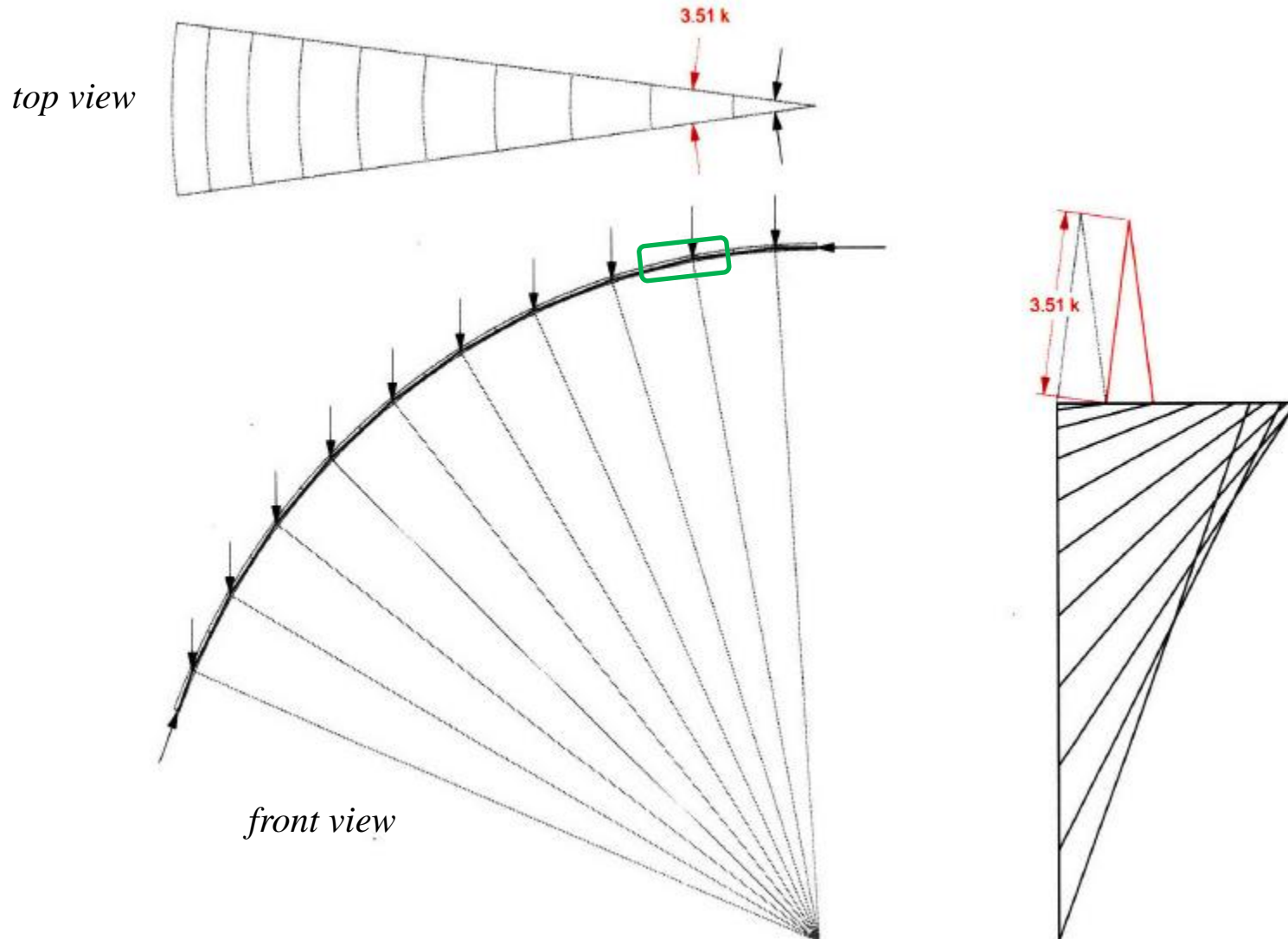


# Wolfe's method, for tension-resisting domes

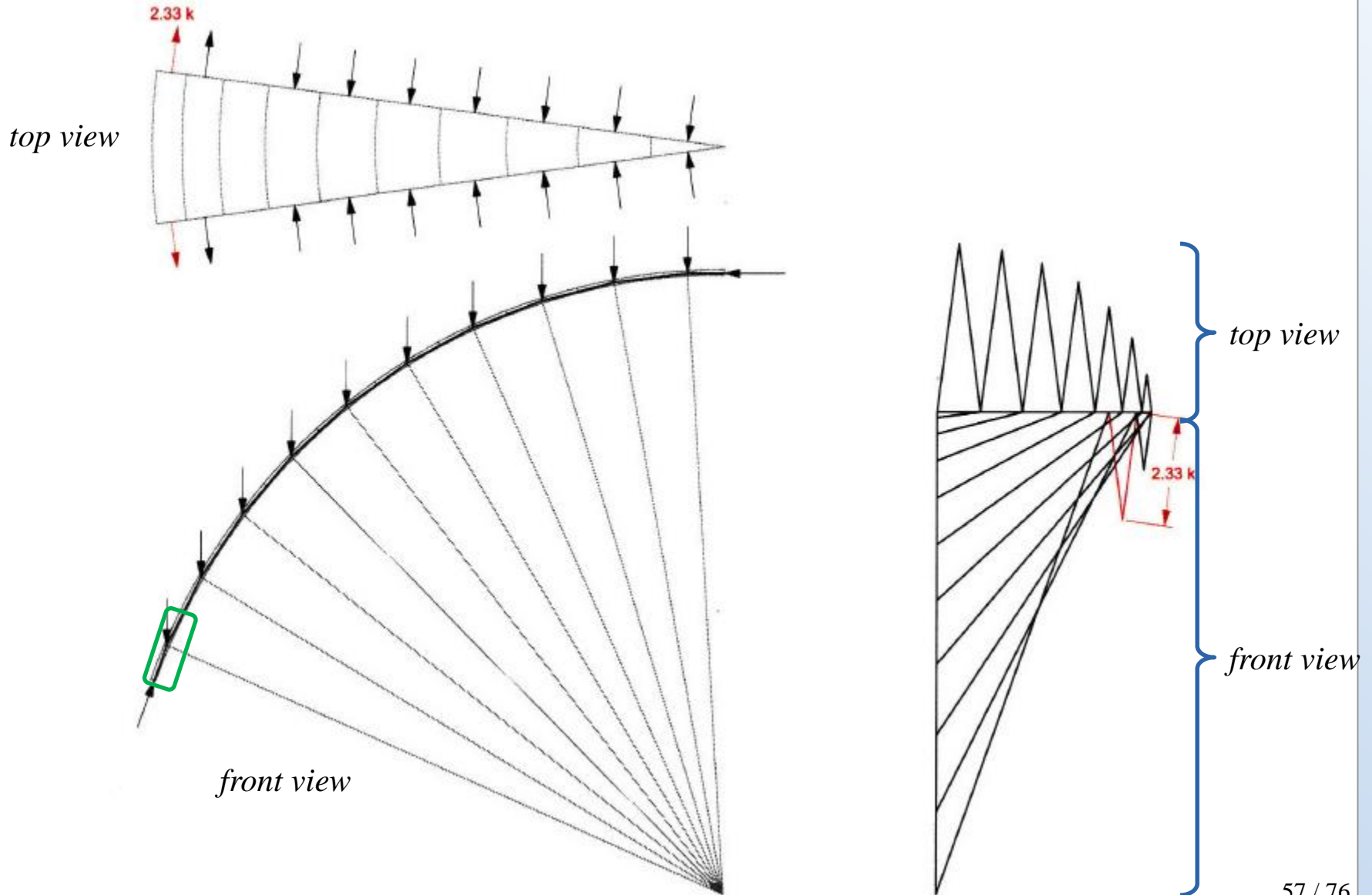




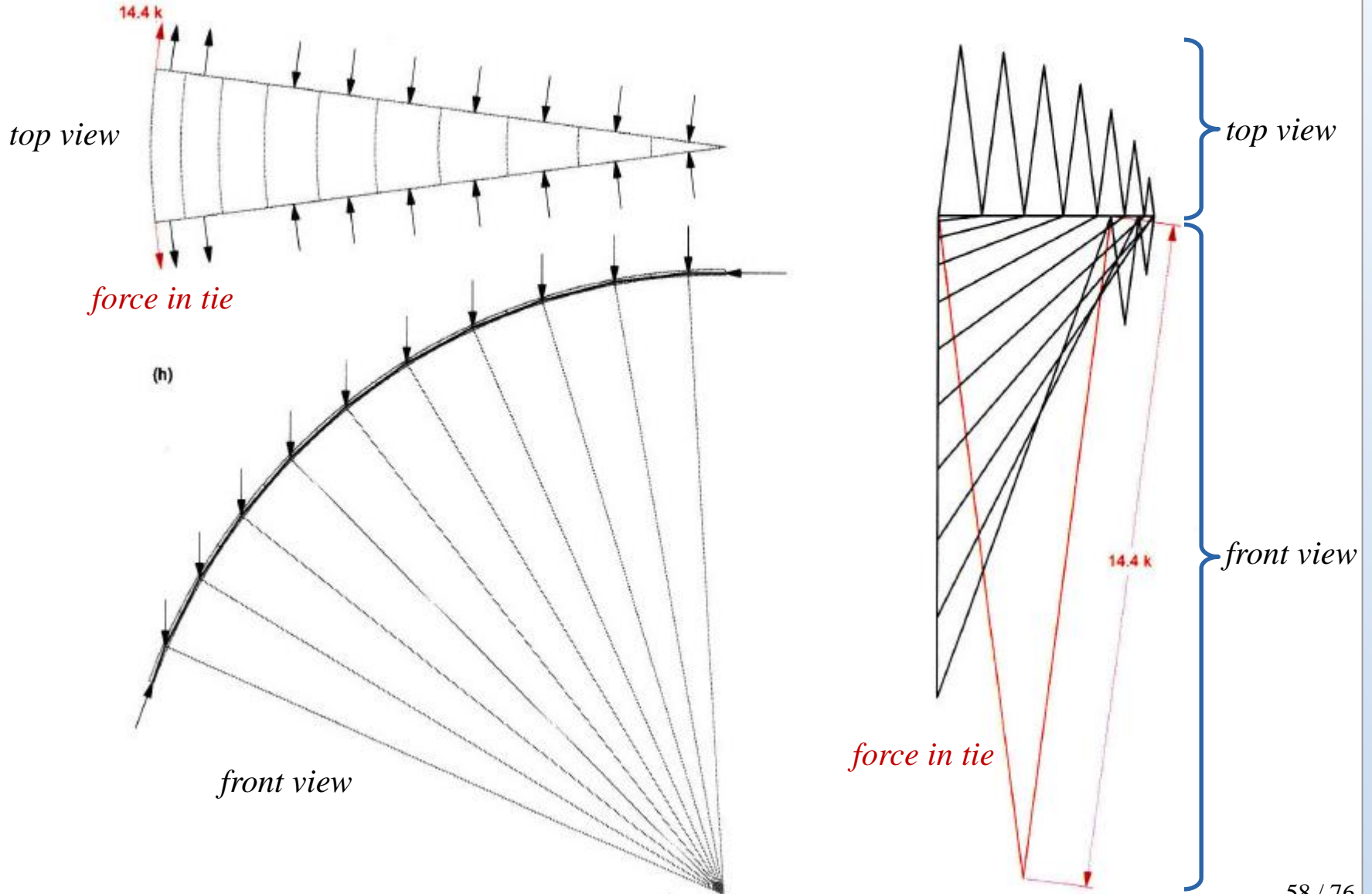
# Wolfe's method, for tension-resisting domes



# Wolfe's method. for tension-resisting domes

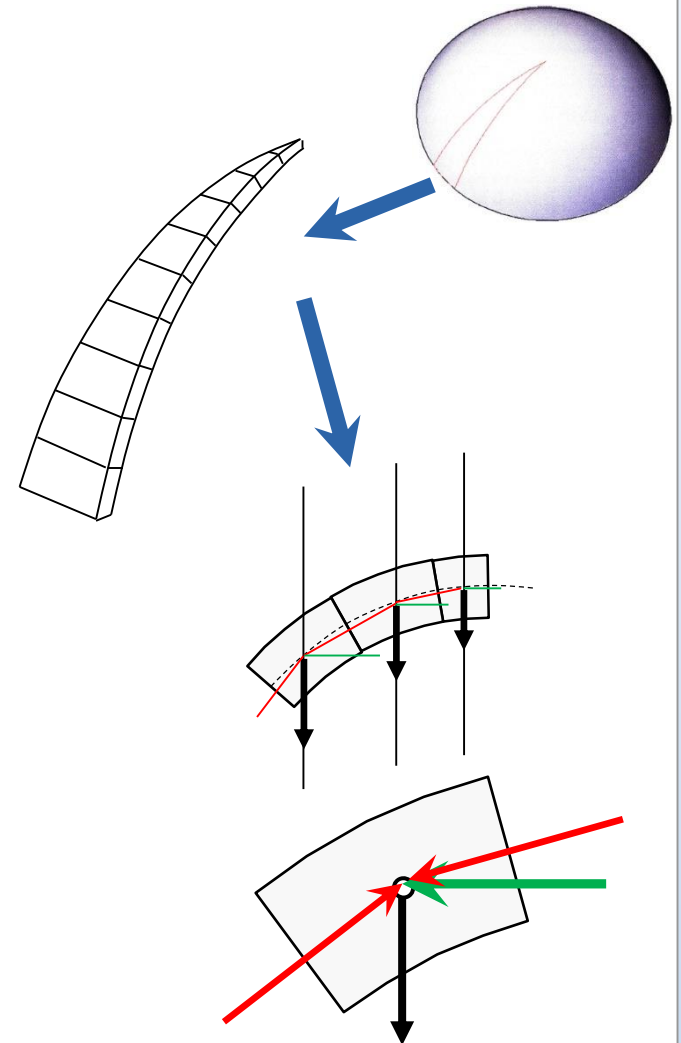


# Wolfe's method, for tension-resisting domes



# Wolfe's method

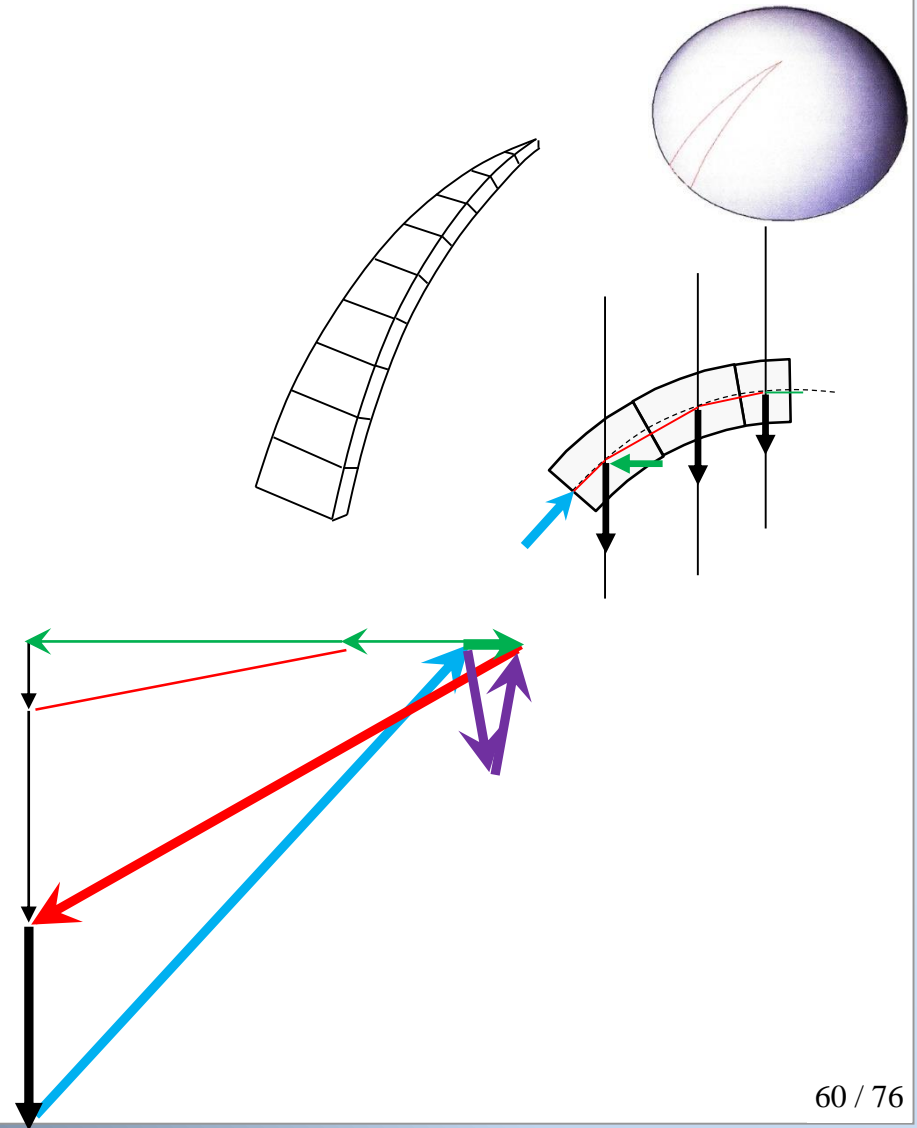
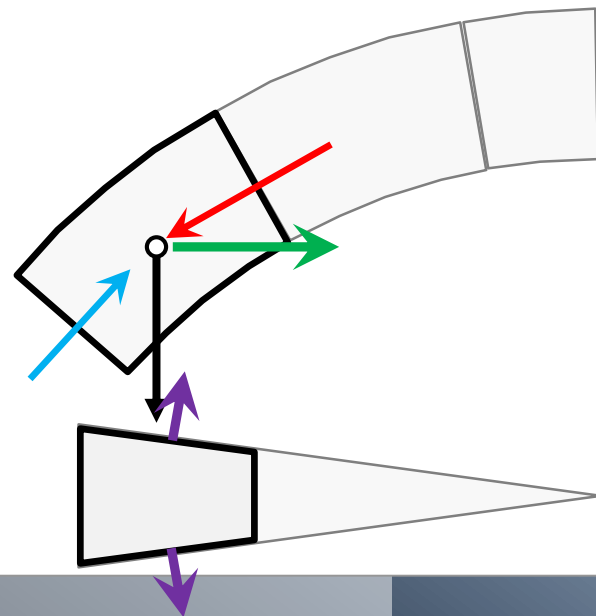
- Version 1.: domes with tension resistance
- Version 2.: domes without tension resistance



# Wolfe's method

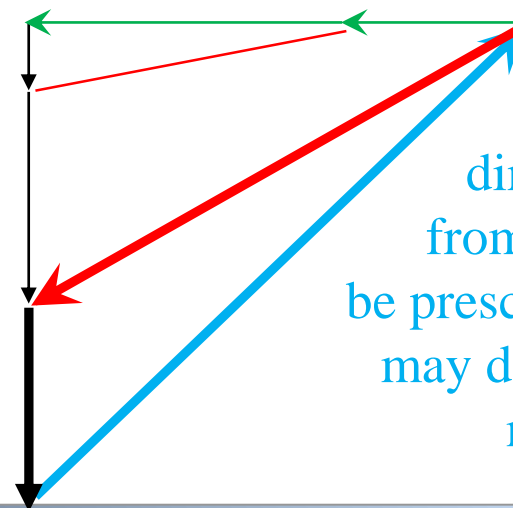
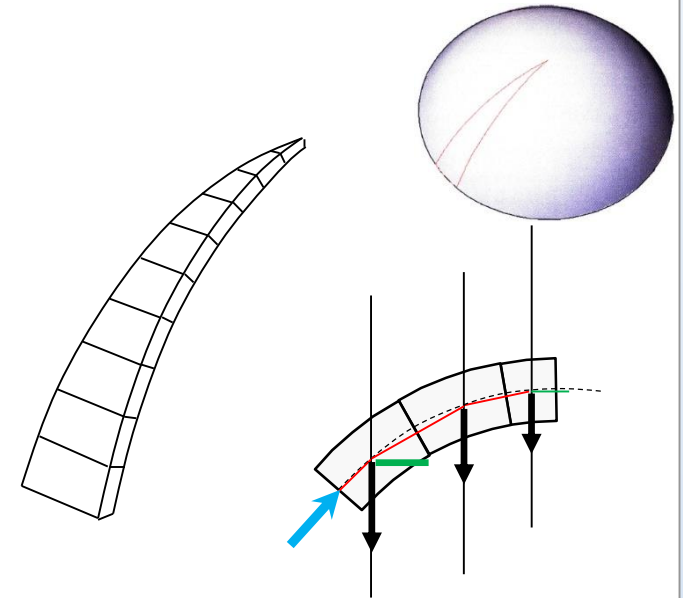
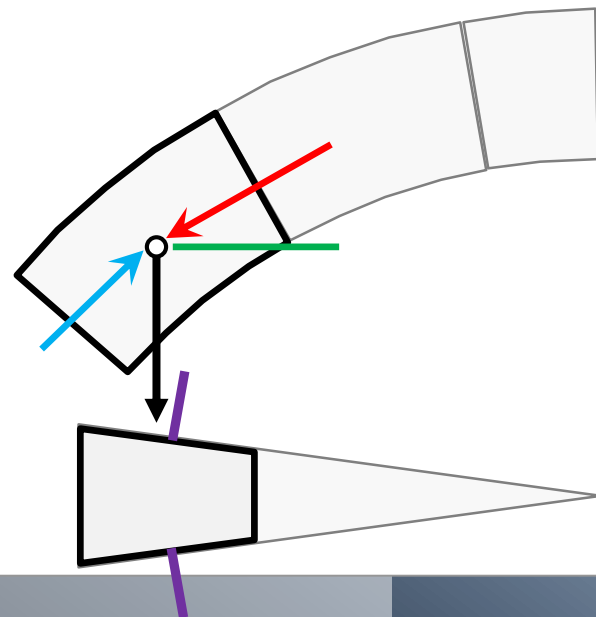
REMEMBER:

3. Analysis of the bottom segment:



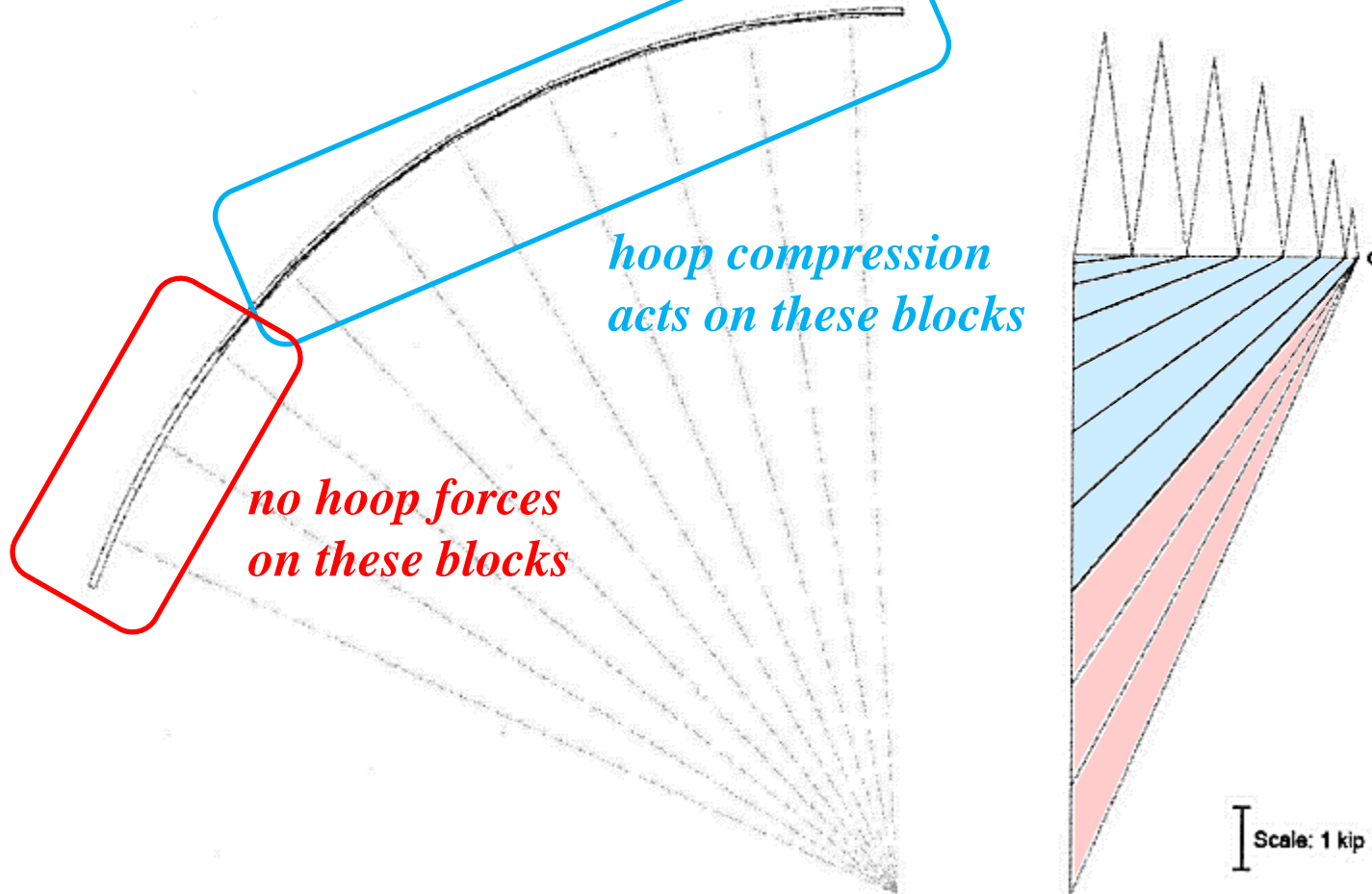
# Wolfe's method, for **no-tension domes**

## 3. Analysis of the bottom segment:



direction of force  
from below: cannot  
be prescribed/assumed:  
may deviate from the  
membrane state

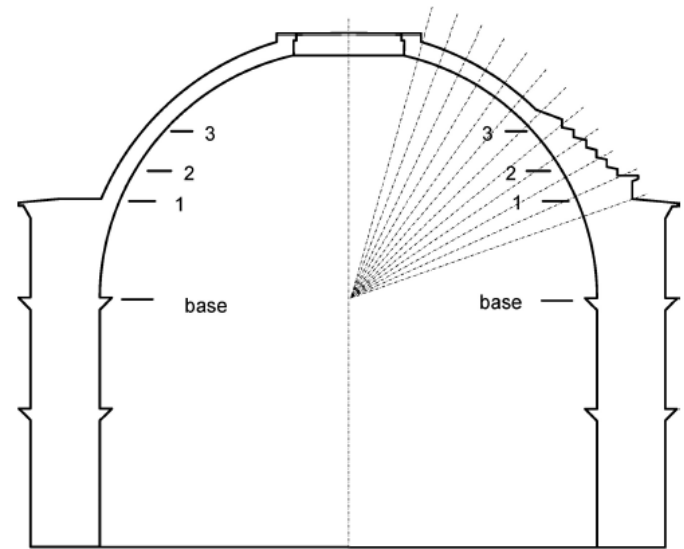
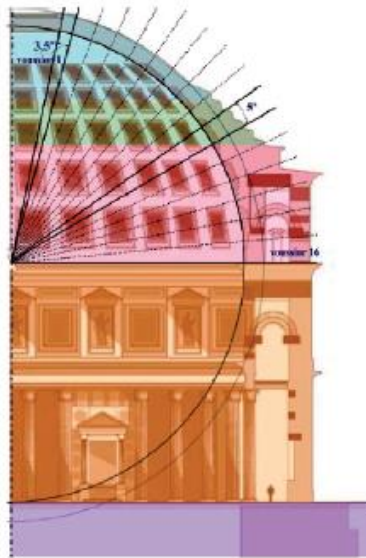
# Wolfe's method, for **no-tension domes**



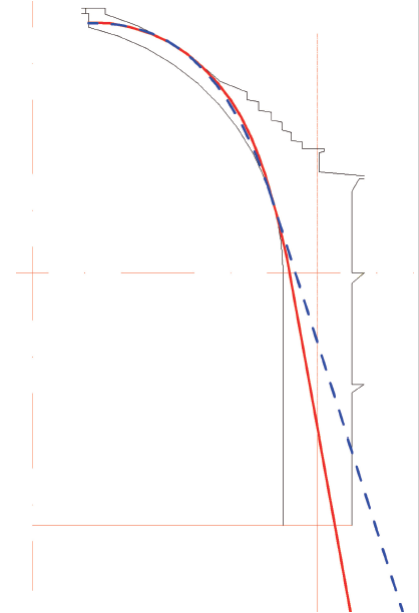
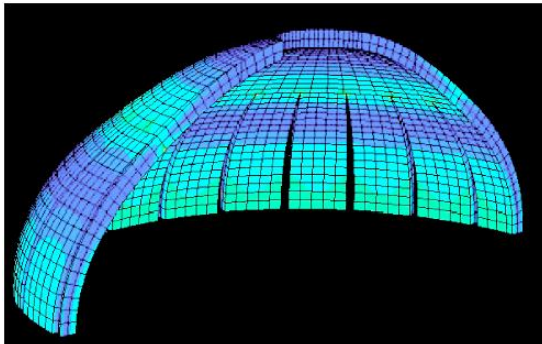
# Wolfe's method

Application:

Morer & Goni (2008):  
Pantheon in Rome, Italy  
[ not masonry! ]



agreement with ABAQUS



method extended to find line of thrust: Lau (2006)



# Wolfe's method

## Application:



*Cavalagli & Gusella (2015)*



*Cavalagli et al (2016)*

## Dome of the „Santa Maria Degli Angeli”

Basilica, Assisi, Italy

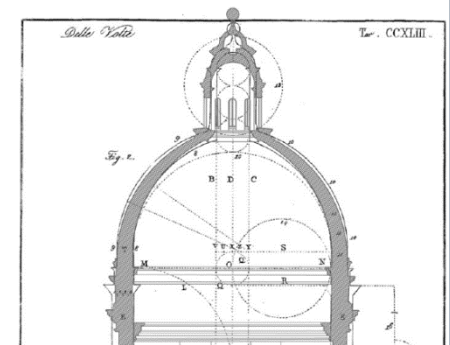
→ construction: 1569-1679; dome completed in 1677

→ dome diameter:  $\approx 20$  m; thickness:  $\approx 180 \dots 90$  cm

perimeter: inside circular, outside octagonal

→ several earthquakes; e.g. 1832

after that: iron rings were added



*Cavalagli et al (2016)*

# Wolfe's method

## Application:



*Cavalagli & Gusella (2015)*

Cavalagli & Gusella (2015):

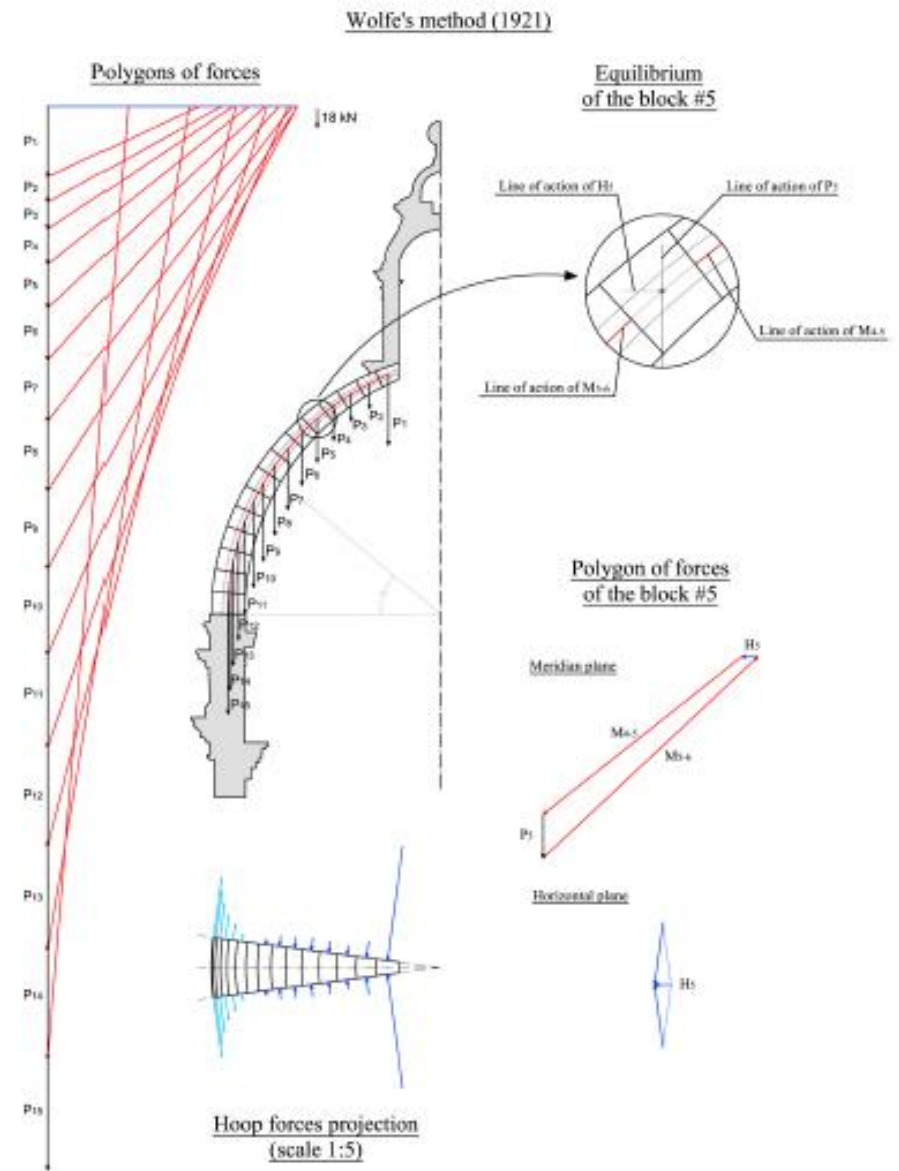
Wolfe's method compared to:

→ the Italian architect manual

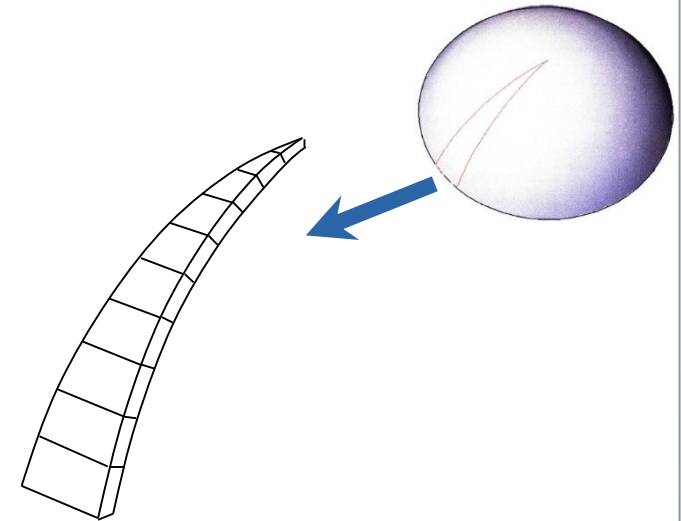
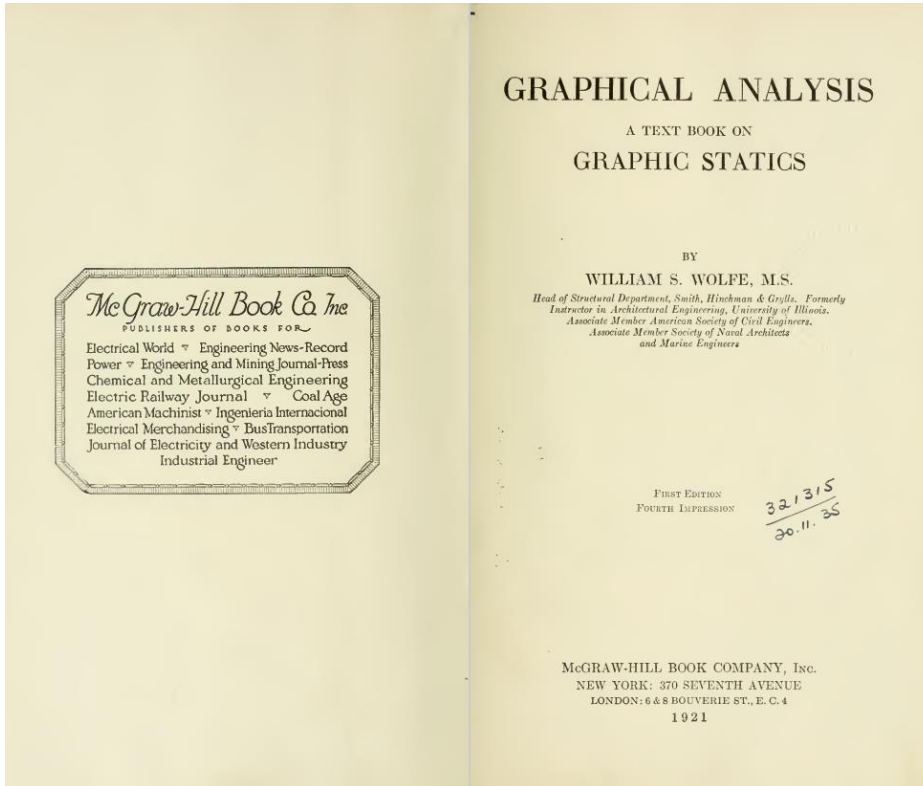
→ another old graphical method;

Conclusion:

graphical methods predict slight  
crackings near the base



# Wolfe's method



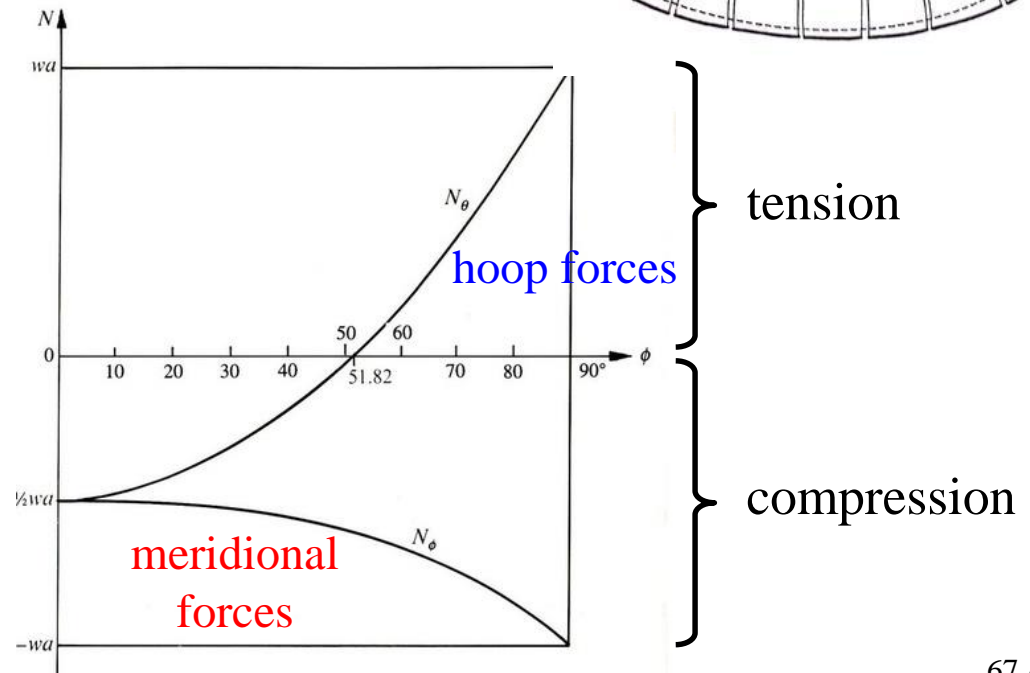
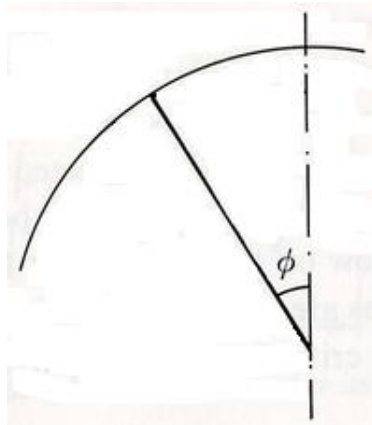
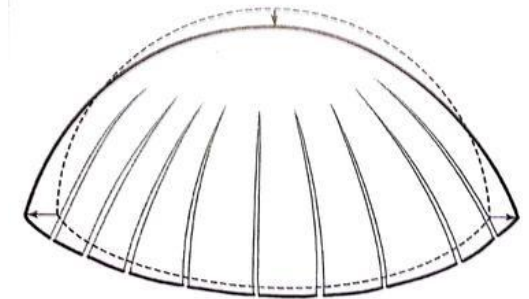
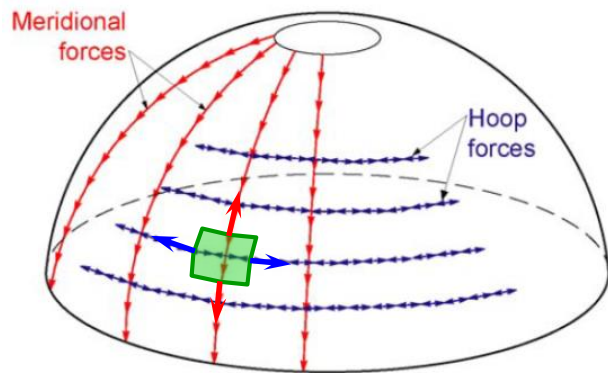
## Further reading:

Wolfe (1921); Reese (2008); Lau (2006);

Cavalagli, N., Gusella, V. (2015); Morer & Goni (2008)

# Remark: Membrane solution for spherical cap

Details: next lecture!



# THIS LECTURE:

## GRAPHICAL METHODS

Historical times: Practical geometrical rules

e.g. Vitruvius

e.g. Gothic rules

### Graphical statics

The basic problem: Stability of an arch

Durand-Claye's stability area method for arches

computerized & extended for domes: Aita et al 2003 ... 2018

Wolfe's method for membrane forces in domes

O'Dwyer's funicular analysis  $\Rightarrow$

Thrust Network Analysis (TNA)

Questions

# Thrust Network Analysis

Preliminary: „Funicular Analysis”, O’Dwyer (1999)

~~masonry vault~~ → 3D truss:      nodes  $\approx$  stone block inner points  
bars  $\approx$  contacts between blocks  
bar forces  $\approx$  contact forces

*Vertical loads only!*

Approximative because:

- all forces acting on a stone block intersect in the same point
- the lines of action in top view must be assumed at the beginning

Given: geometry of the vault; loading forces (dead & live)

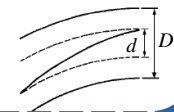
Unknowns:    → vertical coordinates ( $z_i$ ) of the nodes  
                  → some of the horizontal force magnitudes

Equalities: equilibrium of the nodes

Inequalities: nodes fall inside the material:  $z_i^{\text{intrados}} \leq z_i \leq z_i^{\text{extrados}}$

Objective function: either: live load multiplier → max!  
                                  or : deviation from middle surface → min!

*linear  
optimization  
problem*



# Thrust Network Analysis

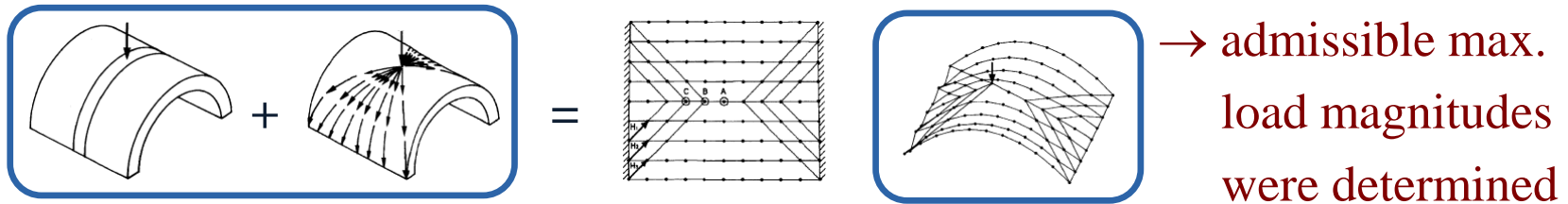
Preliminary: „Funicular Analysis”, O’Dwyer (1999)

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Applications:

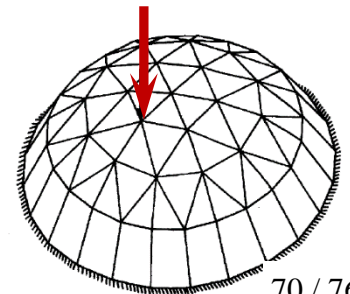
Problem Type 1:

Find maximum admissible live load on a given vault:



Problem Type 2:

Find optimum network shape of a vault under a given load: minimize the vertical deviation of force lines of action from the vault middle surface



# Thrust Network Analysis

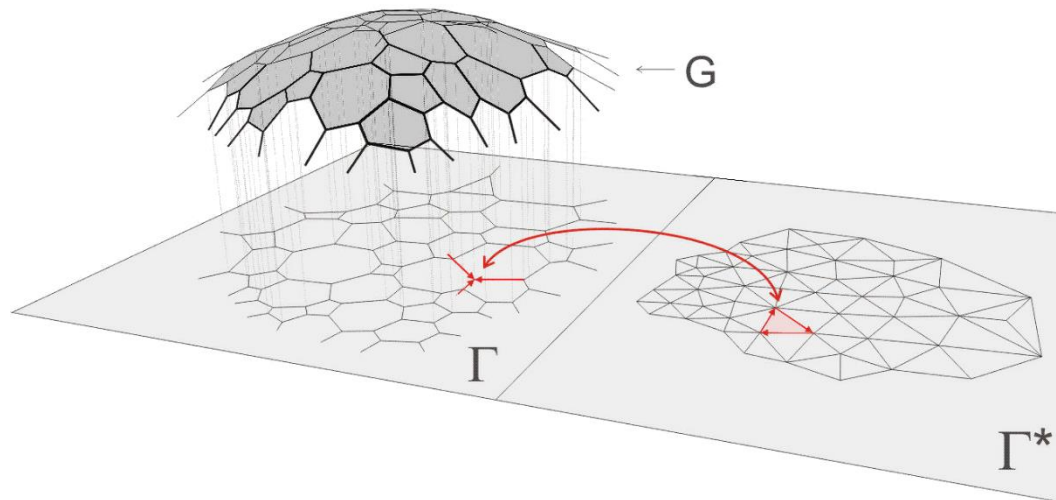
Block & Ochsendorf (2007), (2008); Block & Lachauer (2014):

→ based on O'Dwyer's „Funicular Analysis”

→ sophisticated computer coding; nice graphic representations

objective functions can be:

- (1) minimize deviation from middle surface (max geometrical factor of safety)
- (2) minimal / maximal horizontal thrust (deepest / shallowest force systems)
- (3) maximize live load multiplier which can be added to the given selfweight



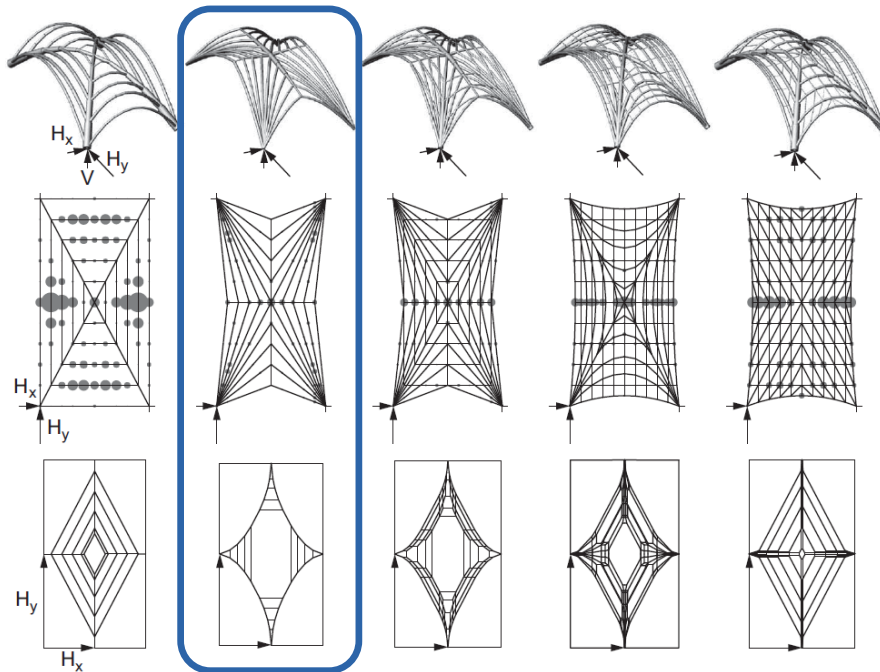


# Thrust Network Analysis

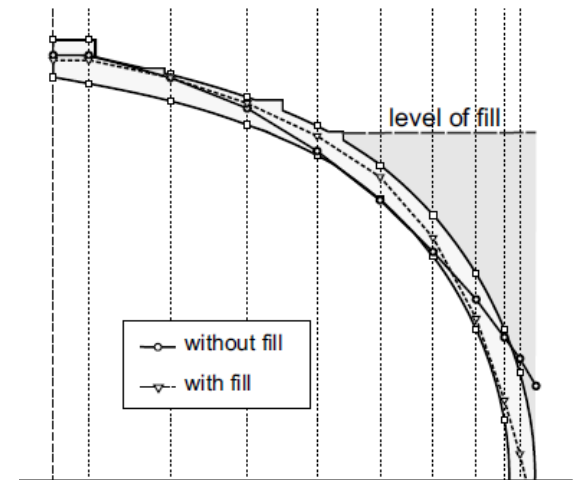
Block & Ochsendorf (2007), (2008); Block & Lachauer (2014):

- based on O'Dwyer's „Funicular Analysis”
- sophisticated computer coding; nice graphic representations
- analysis of several Gothic structures

cross vaults:



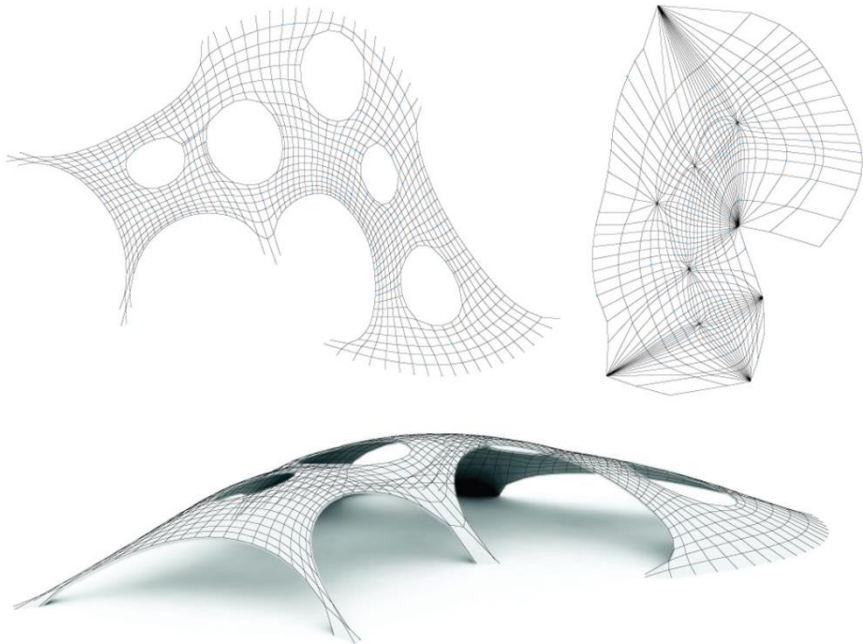
fan vaults:



# Thrust Network Analysis

Block & Ochsendorf (2007), (2008); Block & Lachauer (2014):

- based on O'Dwyer's „Funicular Analysis”
- sophisticated computer coding; nice graphic representations
- analysis of several Gothic structures
- design optimal shapes for vaults



# Thrust Network Analysis

## Block Research Group:

e.g. The Red Line project, Rwanda:

drone port:

tile-vaulted (very thin) structures,  
easy and cheap to construct

„Durabric” (earth + 8% cement, not burnt)

<https://www.youtube.com/watch?v=mZwIIndTUow>



[block.arch.ethz.ch/brg/project/venice-biennale-2016\\_droneport](http://block.arch.ethz.ch/brg/project/venice-biennale-2016_droneport)

# THIS LECTURE:

## GRAPHICAL METHODS

Historical times: Practical geometrical rules

e.g. Vitruvius

e.g. Gothic rules

Graphical statics

The basic problem: Stability of an arch

Durand-Claye's stability area method for arches

computerized & extended for domes: Aita et al 2003 ... 2018

Wolfe's method for membrane forces in domes

O'Dwyer's funicular analysis  $\Rightarrow$

Thrust Network Analysis (TNA)

Questions

# QUESTIONS

1. Introduce a chosen historic geometrical design rule. What is the background for this design rule?
2. How to determine the possible minimal and maximal horizontal thrust for an arch under selfweight, using graphical statics?
3. What is the geometrical factor of safety of an arch or vault?
4. Introduce Durand-Claye's stability area method.
5. Introduce Wolfe's method for domes. How is it used for no-tension material, and for determining the tie force?
6. Introduce the Thrust Network Analysis method. What objective functions can be used?